

# Dynamic Optimization

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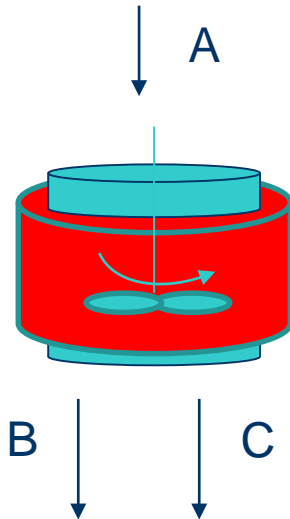
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# Outline

- Dynamic optimization problems
- Parameterization
- Sequential approach
- Simultaneous approach
- Path constraints
- Applications
- Software

# A dynamic system: batch reactor



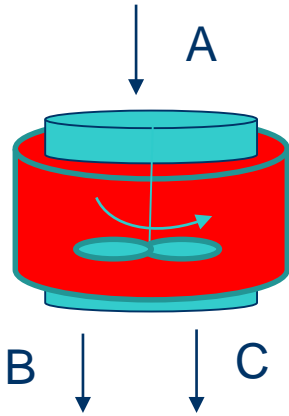
The operation of an endothermic batch reactor last for one hour. It loads an amount A, which reacts according to the parallel reactions  $A \rightarrow B$  and  $A \rightarrow C$ , but only the B product has commercial value. The speeds of reaction are given by:

$$k_B = 10^6 \exp(10000 / RT)$$

$$k_C = 5 * 10^{11} \exp(20000 / RT)$$

Find the temperature profile that maximizes the final production of B, if the temperature must always be bellow 139 °C

# Dynamic Optimization (DO)

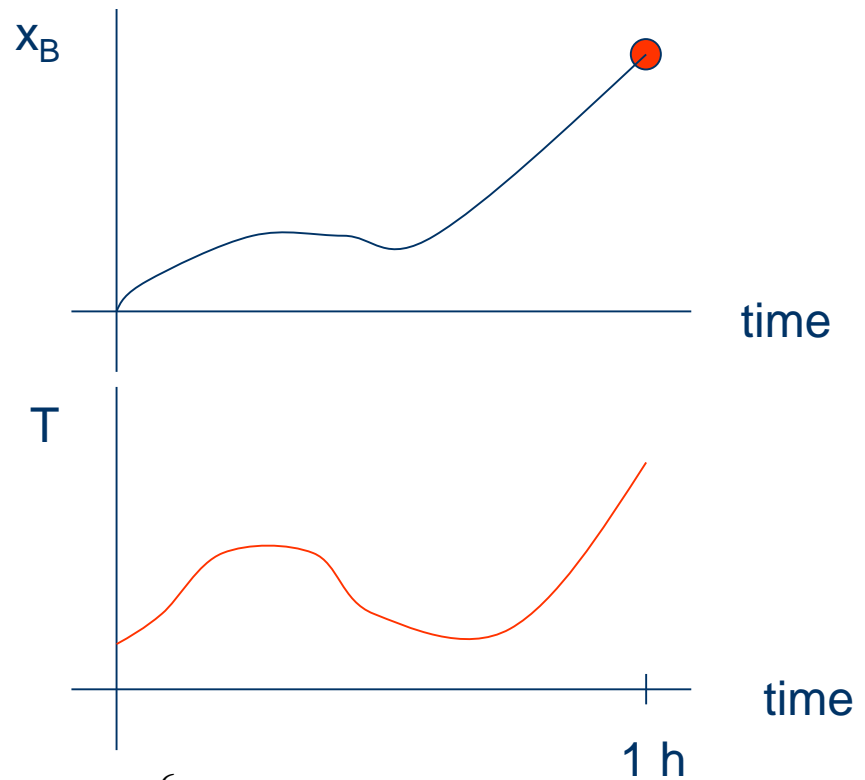


$$\max_{T(t)} x_B(1)$$

$$\frac{dx_A}{dt} = -(k_B + k_C)x_A \quad x_A(0) = A_0$$

$$\frac{dx_B}{dt} = k_B x_A \quad x_B(0) = 0$$

$$T(t) \leq 139$$



$$k_B = 10^6 \exp(10000 / RT)$$

$$k_C = 5 * 10^{11} \exp(20000 / RT)$$

# Dynamic Optimization

$$\min_{\mathbf{u}(t), \mathbf{x}(t), \mathbf{x}_0, t_f} J(\mathbf{u}) = \int_{t_0}^{t_f} C(\mathbf{x}, \mathbf{u}) dt$$

$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{u}, \mathbf{z}), \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

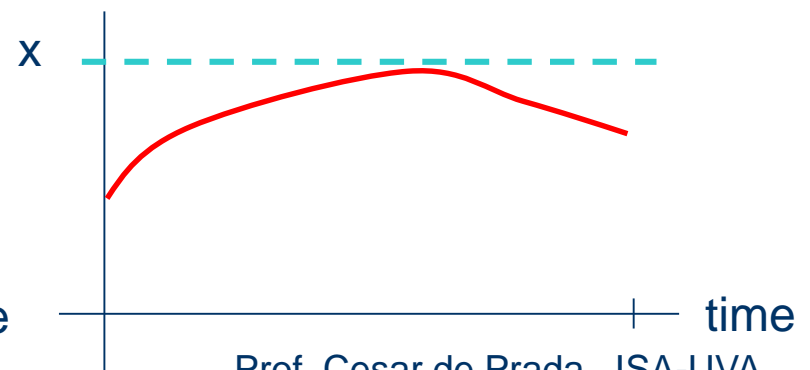
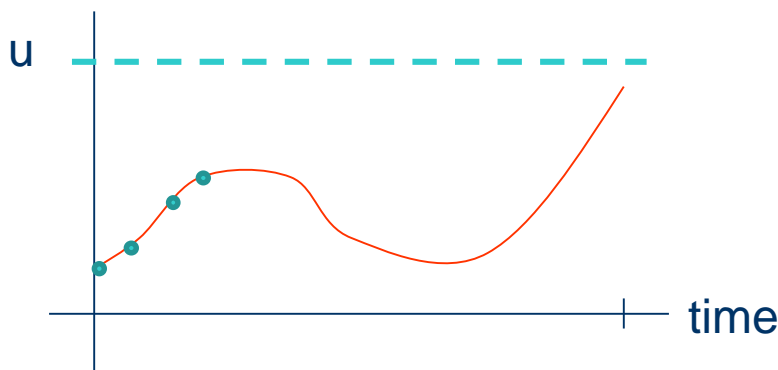
$$\mathbf{h}(\mathbf{x}, \mathbf{u}, \mathbf{z}) = \mathbf{0}$$

$$\mathbf{g}(\mathbf{x}, \mathbf{u}, \mathbf{z}) \leq \mathbf{0}$$

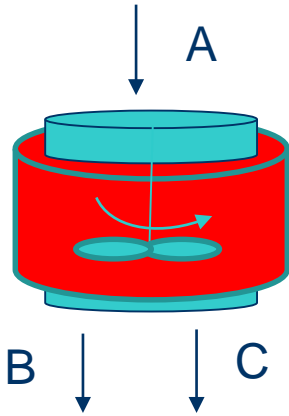
DAE

- ✓ Many types:
  - ✓ Integral or algebraic cost
  - ✓ Initial value problems
  - ✓ TPBV problems
  - ✓ Final time problems
  - ✓ DAE or ODE
  - ✓ ....

Problem: infinite number of decision variables and constraints



# Decision variables parameterization

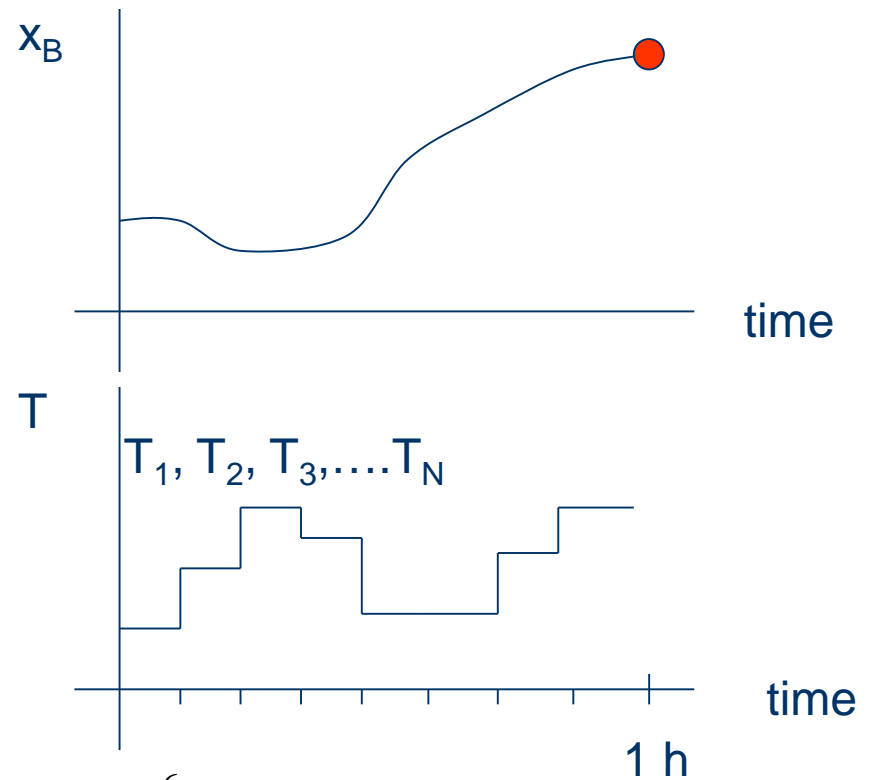


$$\max_{T_i} x_B(1)$$

$$\frac{dx_A}{dt} = -(k_B + k_C)x_A \quad x_A(0) = A_0$$

$$\frac{dx_B}{dt} = k_B x_A \quad x_B(0) = 0$$

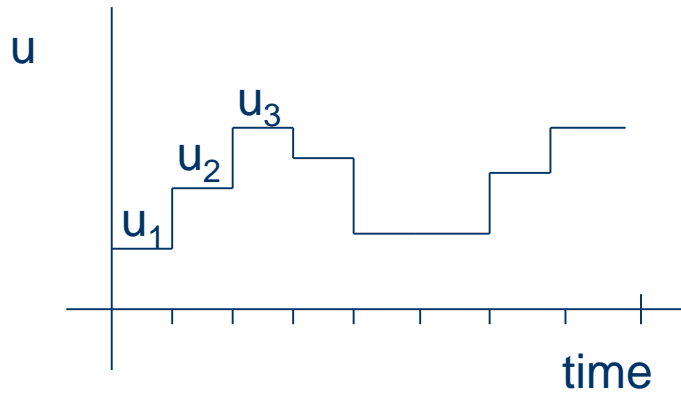
$$T_i \leq 139 \quad i = 0, 1, \dots, N$$



$$k_B = 10^6 \exp(10000 / RT)$$

$$k_C = 5 * 10^{11} \exp(20000 / RT)$$

# Control Vector Parameterization CVP

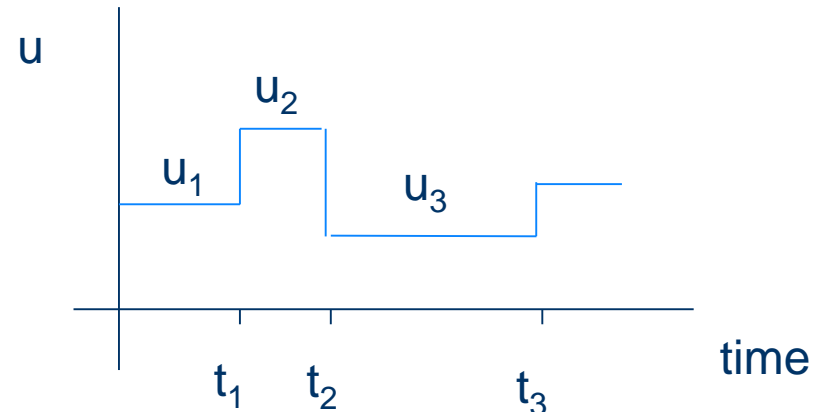
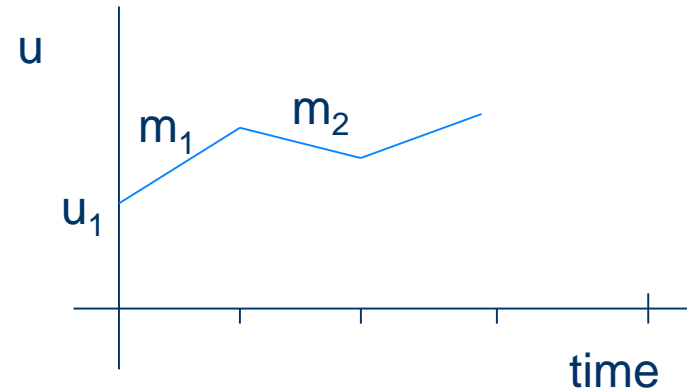


New decision variables

$u_1, u_2, u_3, \dots, u_N$

$u_1, m_1, m_2, \dots, m_N$

$u_1, t_1, u_2, t_2, \dots, u_N, t_N$

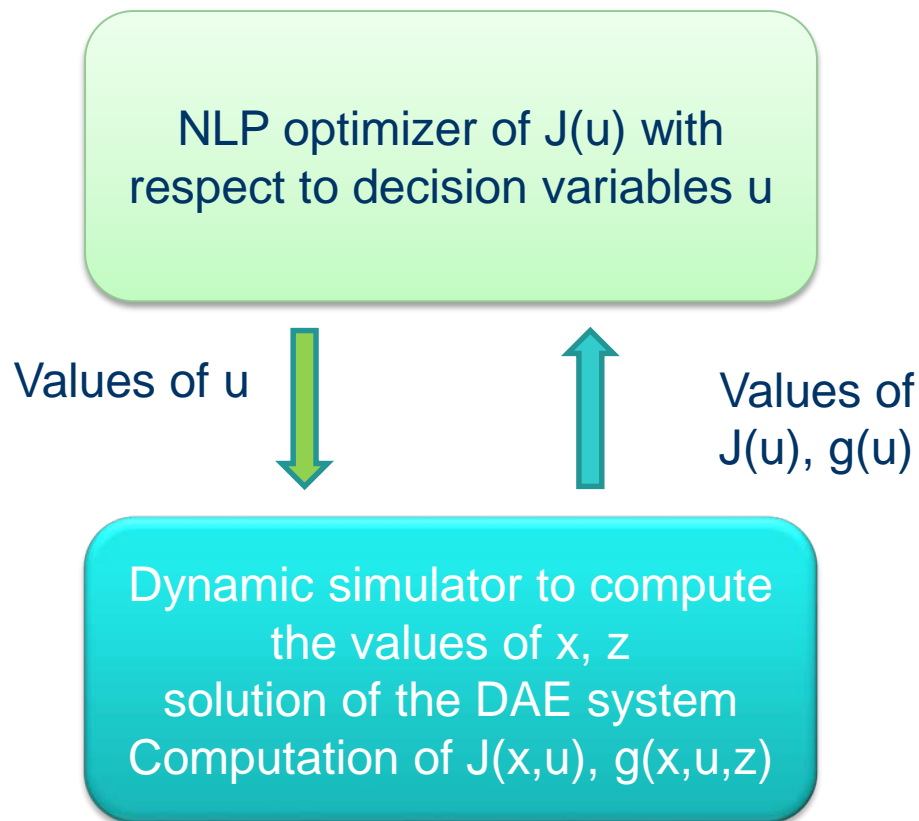


# Solving DO problems

- Two main approaches:
  - Solving the differential equations with a dynamic simulator (Sequential approach) CVP
  - Discretizing the dynamic system to convert it into an algebraic one (Simultaneous approach)
- They are more computational intensive than standard NLP problems



# Sequential approach



$$\min_{u(t), x_0, t_f} J(\mathbf{u}) = \int_{t_0}^{t_f} C(\mathbf{x}, \mathbf{u}) dt$$

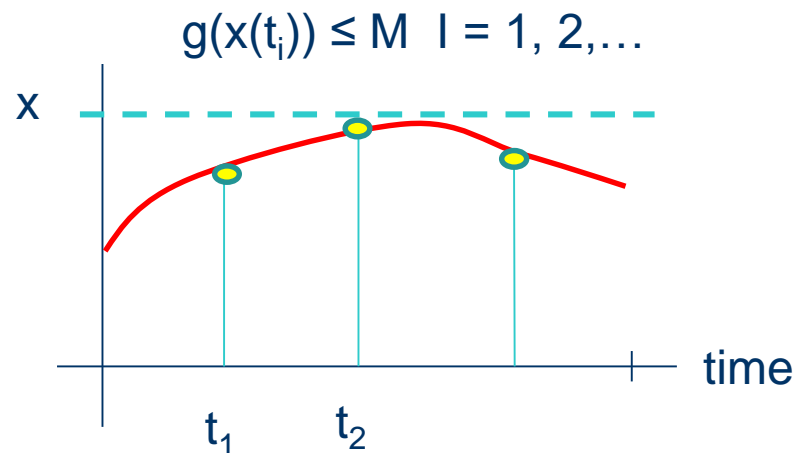
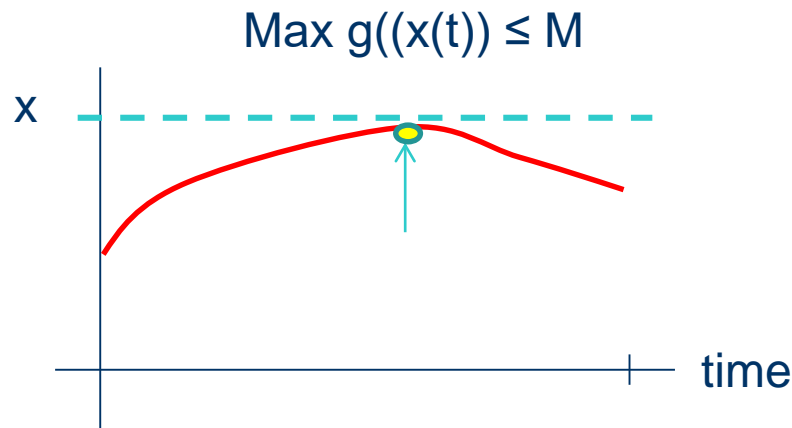
$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{u}, \mathbf{z}), \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

$$\mathbf{h}(\mathbf{x}, \mathbf{u}, \mathbf{z}) = \mathbf{0}$$

$$\mathbf{g}(\mathbf{x}, \mathbf{u}, \mathbf{z}) \leq \mathbf{0}$$

The DO problem is converted into a NLP one, with a number of  $u$  variables equal to the problem degrees of freedom

# Path constraints



The sequential approach uses a smaller number of decision variables (the CVP of  $u$ ) than the simultaneous one, but imposing constraints over time on states and algebraic variables is more difficult as they are computed inside the simulation

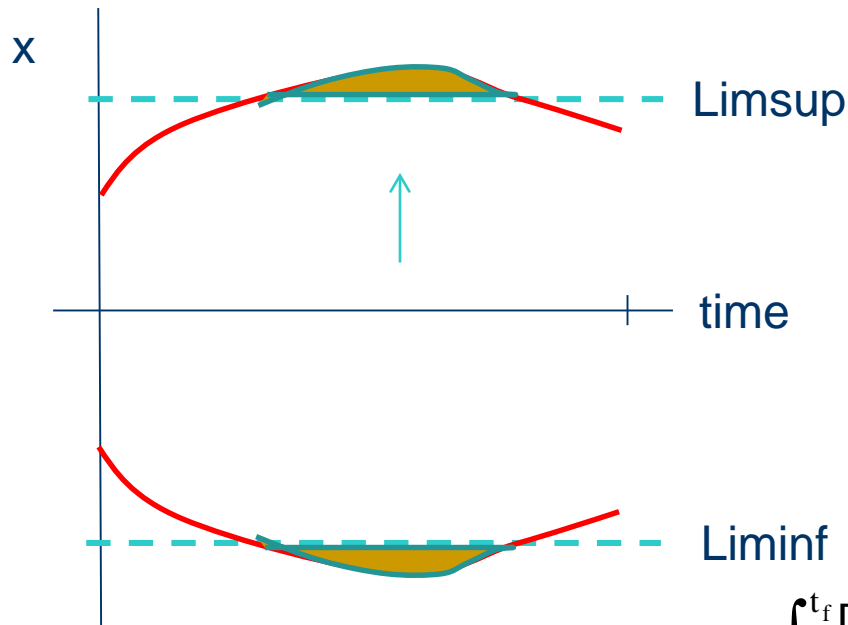
Solutions:

- ✓ Choose several internal points and impose the constraint at this points
- ✓ Compute the max or min of  $x(t)$  and impose the constraint on it

# Path constraints

Another option

$$\int_{t_0}^{t_f} [\max(\text{Lim sup}, \mathbf{x}(t)) - \text{Lim sup}] dt \leq 0$$

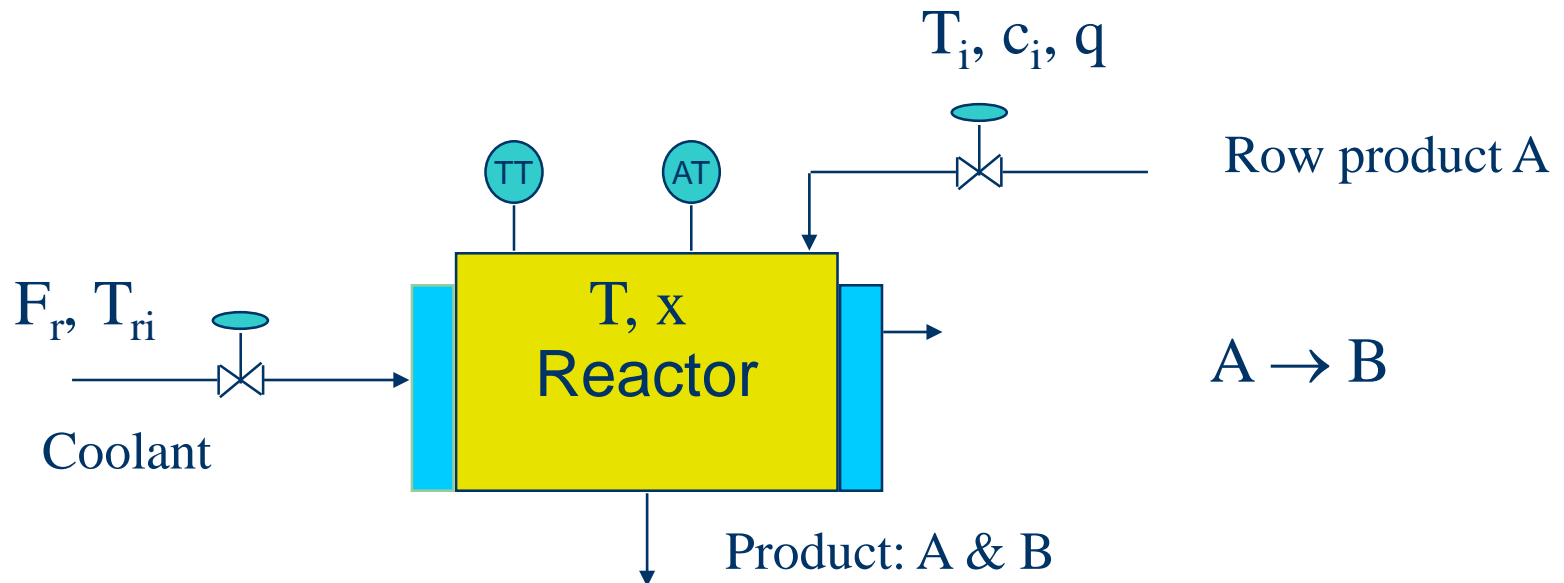


The surface under the trajectory above the upper (or below the lower) limit is constrained to be zero

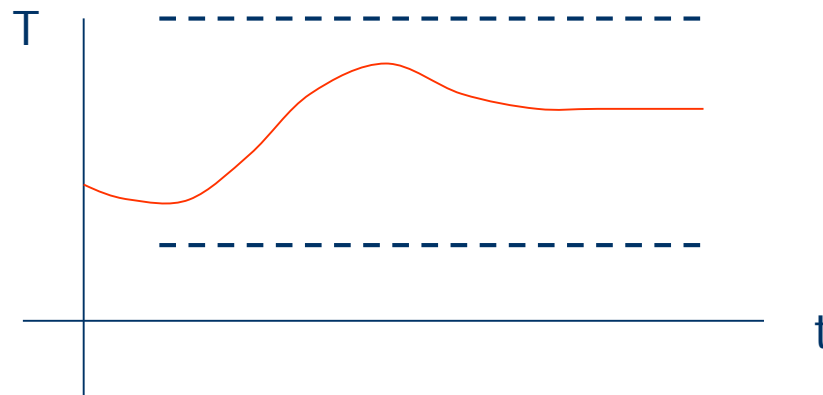
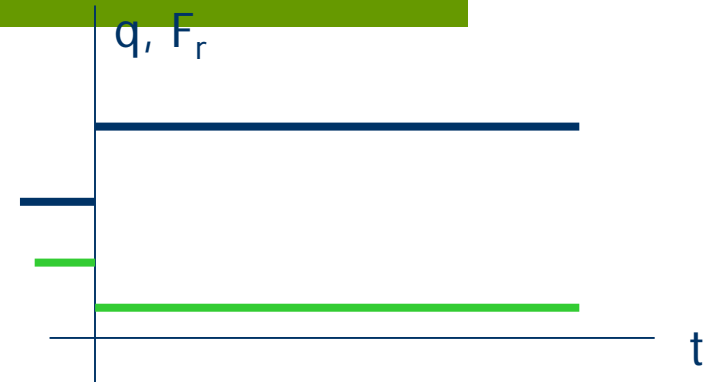
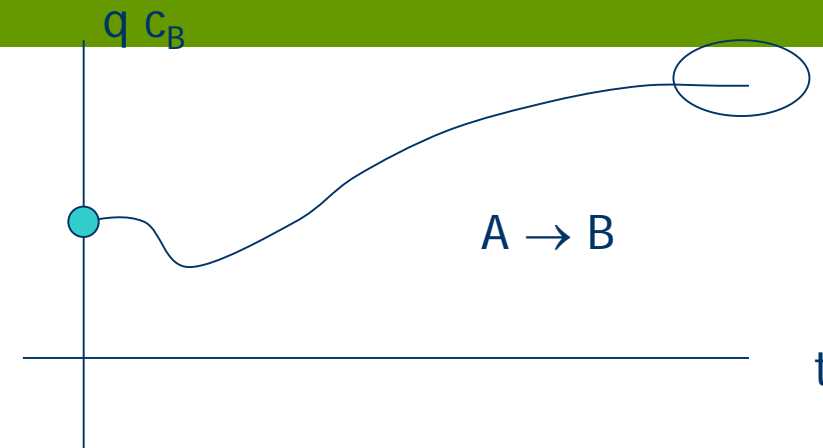
$$-\int_{t_0}^{t_f} [\min(\text{Liminf}, \mathbf{x}(t)) - \text{Liminf}] dt \leq 0$$

# Dynamic Optimization (DO) example

Starting from a certain operation point, and performing a single change in the process MVs, bring the process to the maximum production point respecting a set of constraints over the transient.



# Dynamic Optimization



$x > 0.7$

$$\max_{q, F_r} \int q c_B dt$$

Dynamic model equations

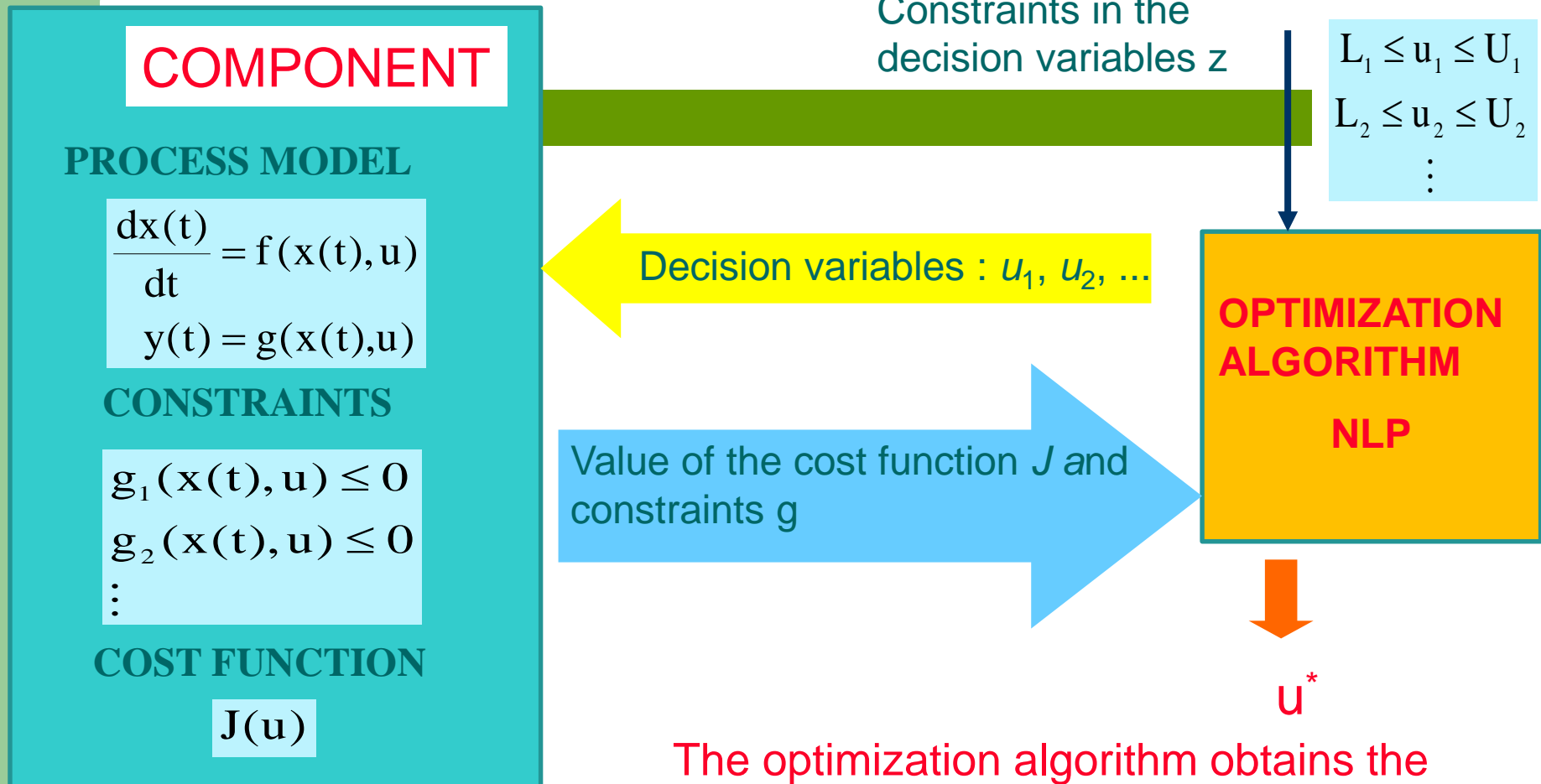
$$\dots \leq q \leq \dots$$

$$\dots \leq F_r \leq \dots$$

$$T_{\min} \leq T(t) \leq T_{\max}$$

# DO in EcosimPro

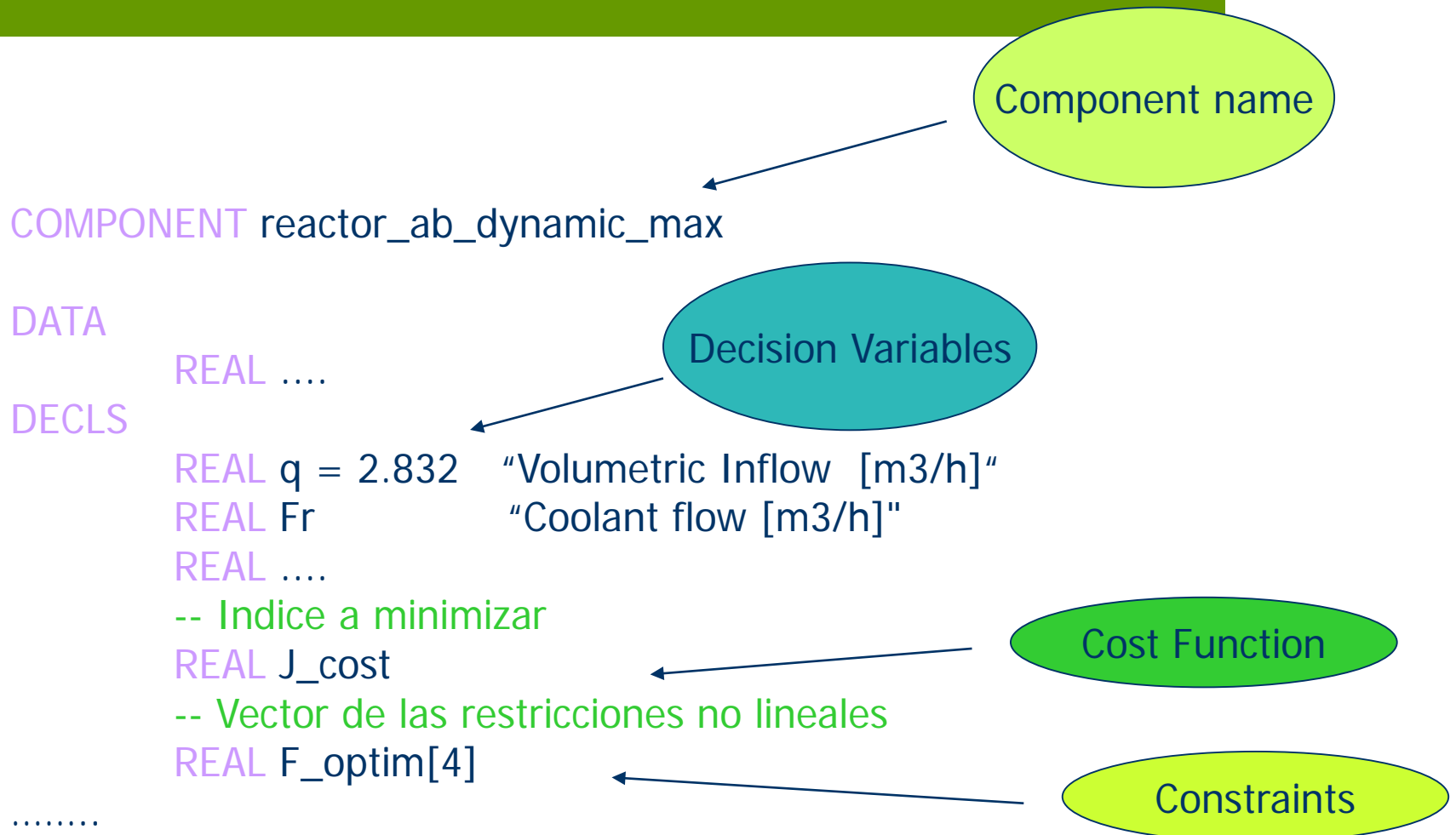
EXPERIMENT



Dynamic simulator

The optimization algorithm obtains the values of the cost function  $J$  and constraints  $g$  when it needs them by calling the dynamic simulation module

# Component / Variables



# Constraints / Cost function

## CONTINUOUS

... ecuaciones del modelo

-- balance de masa de A

$$V \cdot c_A' = q \cdot (c_{A0} - c_A) - V \cdot k \cdot c_A$$

-- balance de energia en el reactor

$$V \cdot \rho \cdot C_p \cdot T' = q \cdot \rho \cdot C_p \cdot (T_e - T) - V \cdot k \cdot c_A \cdot D_H - Q$$

.....

-- calculo de la funcion de costo a minimizar

$$J_{\text{costo}}' = -q \cdot c_B$$

-- calcular las restricciones no lineales (expresiones  $g(x) \leq 0$ )

$$F_{\text{optim}}[1] = J_{\text{costo}}$$

$$F_{\text{optim}}[2] = 0.75 - x$$

$$F_{\text{optim}}[3] = \text{MATH.min}(T, \text{Liminf}T) - \text{Liminf}T$$

$$F_{\text{optim}}[4] = \text{MATH.max}(T, \text{Limsup}T) - \text{Limsup}T$$

END COMPONENT

Dynamic model

Cost function

End point constraint

Path constraint  
 $\text{Max}(T(t)) < \text{Limsup}T$



# Experiment /Functions

```
USE OPTIM_METHODS
```

```
EIDAS calculoSens
```

```
CONST INTEGER numC = 3      -- numero de restricciones del problema
```

```
CONST INTEGER numU = 2      -- numero de variables de decisión
```

```
--CONST INTEGER numX = 4    -- número de variables de estado + 1 (costo)
```

```
FUNCTION INTEGER coste_y_restricciones (IN REAL esnopt_x[], IN  
INTEGER needF, OUT REAL esnopt_F[], IN INTEGER explicit_derivatives,  
IN INTEGER needG, OUT REAL esnopt_G[])
```

```
.....
```

```
END FUNCTION
```

# Experiment / Functions

```
FUNCTION NO_TYPE funcionResiduos( ..... )
```

```
.....
```

```
END FUNCTION
```

```
FUNCTION NO_TYPE funcionCuadraturas( ..... )
```

```
.....
```

```
-- funciones de cuadraturas, fijar la dimension de F_optim
```

```
FOR( i IN 1,4 )
```

```
    quad[i] = F_optim[i]
```

```
END FOR
```

```
END FUNCTION
```

```
FUNC_PTR<ptrFunRes> ptrRes = funcionResiduos
```

```
FUNC_PTR<ptrFunRes> ptrQuad = funcionCuadraturas
```

# Experiment / Variables

```
EXPERIMENT optim ON reactor_ab_dynamic_max.open_loop
```

## DECLS

```
REAL dec_var[numU]      -- valor inicial de las variables de decision
REAL xlow[numU]         -- valor inferior de las variables de decision
REAL xupp[numU]         -- valor superior de las variables de decision
REAL Flow[numC + 1]    -- valor inferior de la funcion objetivo y las
                        -- restricciones
REAL Fupp[numC + 1]    -- valor superior de la funcion objetivo y las
                        -- restricciones
INTEGER calcularSens = 1 -- igual a 1 si se calculan sensibilidades
INTEGER infoESnopt = 0  -- informacion interna de SNOPT
```

## OBJECTS

```
VECTOR_STRING nombresX -- variable auxiliar para la inicialización de
                        -- las sensibilidades
```

# Experiment / INIT

## INIT

-- initial values for state variables

$$cA = 2.891$$

$$Tr = 51.5$$

$$T = T0$$

$$J\_coste = 0$$

## BOUNDS

-- Set equations for boundaries: boundVar = f(TIME;...)

$$Fr = 50$$

$$q = 2$$

# Experiment

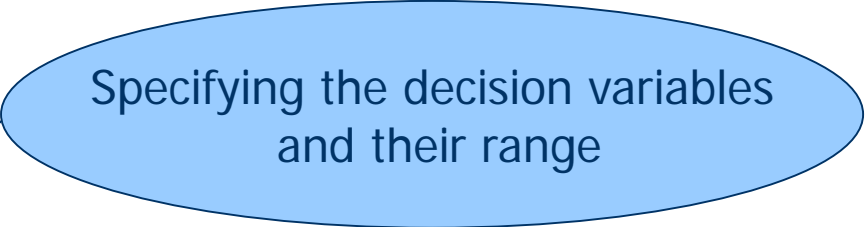
BODY

.....

-- inicialización de las variables de decisión, y los límites  
-- addU( nombre de la variable, valor inicial de la misma,  
booleano que indica si el parámetro es un valor inicial )

```
calculoSens.addU( "q", q, FALSE )  
calculoSens.addU( "Fr", Fr, FALSE )
```

```
dec_var[1] = q  
dec_var[2] = Fr  
xlow[1] = 0.5  
xupp[1] = 5  
xlow[2] = 5  
xupp[2] = 90
```



Specifying the decision variables  
and their range

# Experiment

TIME = 0

TSTOP = 10

CINT = 0.1

-- Inicializacion del algoritmo de integracion y cálculo de sensibilidades

.....  
-- Configurar la tolerancia en el cálculo de sensibilidades (opcional)

    calculoSens.setTol( 1e-5 )

-- inicialización de los límites de las restricciones y la función de coste

    Flow[1] = -1.0e6

    Fupp[1] = 1.0e6

    Flow[2] = Liminfx

-- End point constraint

    Fupp[2] = 1

-- End point constraint

    Flow[3] = 0

-- Path constraint

    Fupp[3] = 0

-- Path constraint

    Flow[4] = 0

    Fupp[4] = 0

# Experiment /SNOPT

```
esnopt_init (numU, numC)
esnopt_set_variables_bounds_and_initial_values (xlow, xupp, dec_var)
esnopt_set_constraints_bounds_and_initial_values (Flow, Fupp, F_optim)
esnopt_set_cost_function_and_constraints (coste_y_restricciones)
esnopt_set_explicit_derivatives ( calcularSens )
esnopt_set_function_precision ( 1.0e-5 )
esnopt_set_iterations_limit (200)
infoESnopt = esnopt
```

Calling the optimizer

-- Final de la optimización, obtención de los resultados para la simulacion.

```
setSilentMode(FALSE)
SET_REPORT_ACTIVE("#MONITOR",TRUE)
esnopt_print_data ()
esnopt_get_variables_values(dec_var)
esnopt_free ()
```

Getting the solution

# Experiment

-- Llamada al integrador

RESET()

-- Modificación de los parámetros con los nuevos valores obtenidos

q = dec\_var[1]

Fr = dec\_var[2]

TIME = 0

CINT = 0.1

INTEG()

.....

END EXPERIMENT



# Cost and constraints

```
FUNCTION INTEGER coste_y_restricciones (IN REAL esnopt_x[], , IN  
INTEGER needF, OUT REAL esnopt_F[], IN INTEGER explicit_derivatives, IN  
INTEGER needG, OUT REAL esnopt_G[])
```

```
  DECLS
```

```
    .....
```

```
  BODY
```

```
    .....
```

```
-- Actualizar las variables de decisión a los valores que propone el optimizador
```

```
  calculoSens.setU( "q", esnopt_x[1] )
```

```
  calculoSens.setU( "Fr", esnopt_x[2] )
```

```
  .....
```

# Cost and Constraints

```
-- Introduccion de los gradientes de la funcion de costo y restricciones a SNOPT
-- si la funcion es de camino, hay que introducir la derivada parcial de la cuadratura
-- ( arr_quadsen ), en caso contrario, si la restricción es de punto final, al usar
-- arr_quadsen_p se usa la derivada parcial del valor de la función.
```

```
IF ( explicit_derivatives == 1) THEN
```

```
-- derivadas de las 4 F_optim respecto a las 2 variables de decision
```

```
esnopt_G[1] = arr_quadsen[ 1 ] -- der(F-optim[1]/d q
```

```
esnopt_G[2] = arr_quadsen[ 2 ] -- der(F-optim[1]/d Fr
```

```
esnopt_G[3] = arr_quadsen_p[ 3 ] -- der(F-optim[2]/d q
```

```
esnopt_G[4] = arr_quadsen_p[ 4 ] -- der(F-optim[2]/d Fr
```

```
esnopt_G[5] = arr_quadsen[ 5 ]
```

```
esnopt_G[6] = arr_quadsen[ 6 ]
```

```
esnopt_G[7] = arr_quadsen[ 7 ]
```

```
esnopt_G[8] = arr_quadsen[ 8 ]
```

# Cost and Constraints

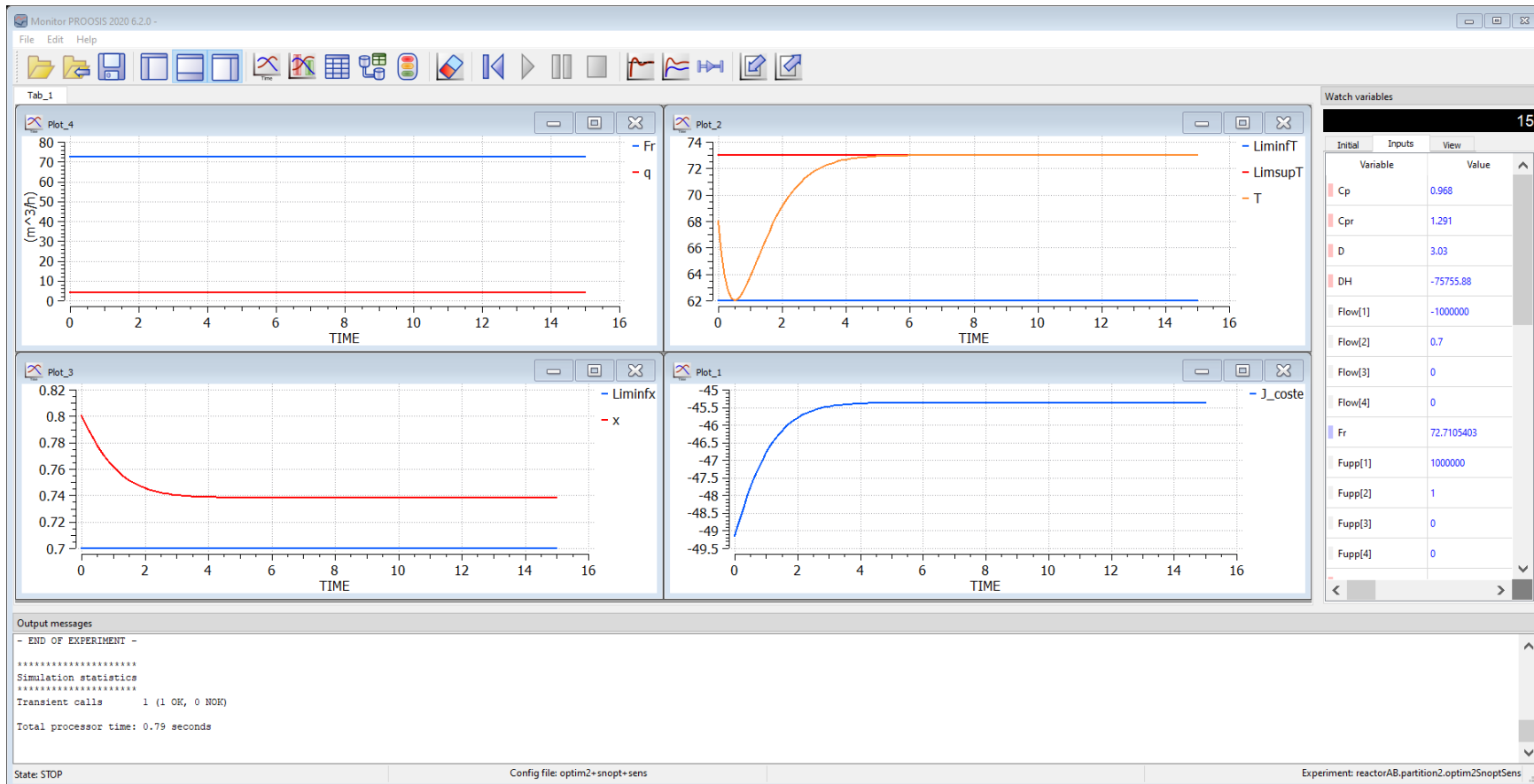
- Introducción de los valores de las funciones a SNOPT
- si la función es de camino, hay que introducir la cuadratura ( arr\_quad )
- en caso contrario, si la restricción es de punto final, al usar F\_optim se
- usa el valor de la función.

```
esnopt_F[1] = arr_quad[1]  
esnopt_F[2] = F_optim[2]  
esnopt_F[3] = arr_quad[3]  
esnopt_F[4] = arr_quad[4]
```

```
RETURN 0
```

```
END FUNCTION
```

# Results in EcosimPro (EcoMonitor)



# Simultaneous approach

- It is based in the discretization of the equations

$$\min_{\mathbf{u}(t), \mathbf{x}(t), \mathbf{x}_0, t_f} J(\mathbf{u}) = \int_{t_0}^{t_f} C(\mathbf{x}, \mathbf{u}) dt$$

$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{u}, \mathbf{z}), \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

$$\mathbf{h}(\mathbf{x}, \mathbf{u}, \mathbf{z}) = \mathbf{0}$$

$$\mathbf{g}(\mathbf{x}, \mathbf{u}, \mathbf{z}) \leq \mathbf{0}$$



$$\min_{\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k} J = \sum_{j=1}^N C(\mathbf{x}_k, \mathbf{u}_k) \Delta_k$$

$$\mathbf{x}_{k+1} = \tilde{\mathbf{f}}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k)$$

$$\mathbf{h}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k) = \mathbf{0}$$

$$\mathbf{g}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k) \leq \mathbf{0}$$

$$k = 0, 1, 2, \dots, N$$

The discretized model has only algebraic equations and can be solved with NLP methods.

# Discretization

One important problem associated with the simultaneous approach is the discretization of the differential equations

$$\min_{\mathbf{u}(t), \mathbf{x}(t), \mathbf{x}_0, t_f} \mathbf{J}(\mathbf{u}) = \int_{t_0}^{t_f} \mathbf{C}(\mathbf{x}, \mathbf{u}) dt$$

$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{u}, \mathbf{z}), \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

$$\mathbf{h}(\mathbf{x}, \mathbf{u}, \mathbf{z}) = 0$$

$$\mathbf{g}(\mathbf{x}, \mathbf{u}, \mathbf{z}) \leq 0$$

Simple methods, such as the Euler discretization are not robust and lead to numerical problems with stiff systems

$$\frac{d\mathbf{x}}{dt} \approx \frac{\mathbf{x}(t + \Delta_t) - \mathbf{x}(t)}{\Delta_t} = \frac{\mathbf{x}_{k+1} - \mathbf{x}_k}{\Delta_t}$$

$$\mathbf{x}_{k+1} = \mathbf{x}_k + \mathbf{f}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k) \Delta_t$$

Other methods such as higher order implicit integration ones or collocation methods should be used

# Simultaneous approach

$$\min_{\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k} J = \sum_{j=1}^N C(\mathbf{x}_k, \mathbf{u}_k) \Delta_k$$

$$\mathbf{x}_{k+1} = \tilde{\mathbf{f}}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k)$$

$$\mathbf{h}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k) = 0$$

$$\mathbf{g}(\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k) \leq 0$$

$$k = 0, 1, 2, \dots, N$$



$$\min_{\mathbf{x}_k, \mathbf{u}_k, \mathbf{z}_k} J = \sum_{j=1}^N C(\mathbf{x}_k, \mathbf{u}_k) \Delta_k$$

$$\mathbf{x}_1 = \tilde{\mathbf{f}}(\mathbf{x}_0, \mathbf{u}_0, \mathbf{z}_0)$$

$$\mathbf{x}_2 = \tilde{\mathbf{f}}(\mathbf{x}_1, \mathbf{u}_1, \mathbf{z}_1)$$

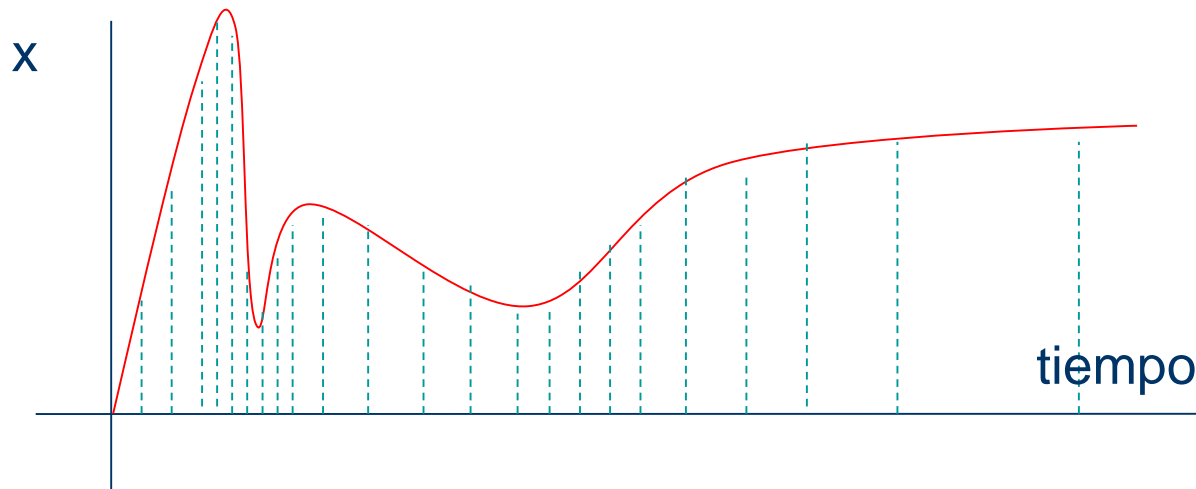
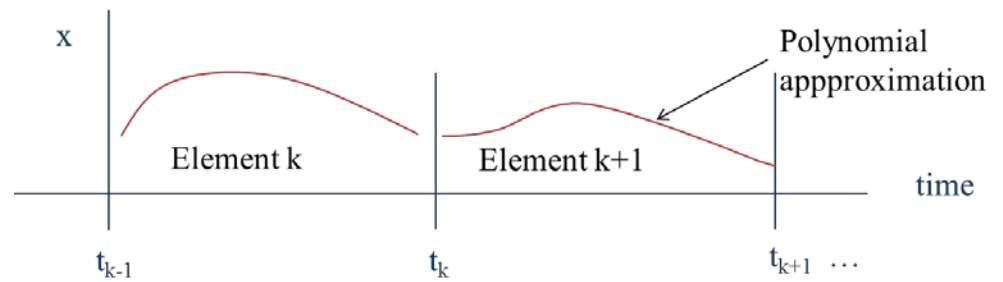
$$\mathbf{x}_3 = \tilde{\mathbf{f}}(\mathbf{x}_2, \mathbf{u}_2, \mathbf{z}_2)$$

.....

The number of equations increases by a factor of  $N$  and the number of decision variables increases from the CVP of  $u$  to  $u_k, x_k, z_k$  with respect to the sequential approach

But it is easier to impose constraints on the time evolution of the states and algebraic variables (path constraints) by limiting  $x_k, z_k$  at the discretization points

# Discretización



**Colocación  
ortogonal por  
elementos  
finitos**

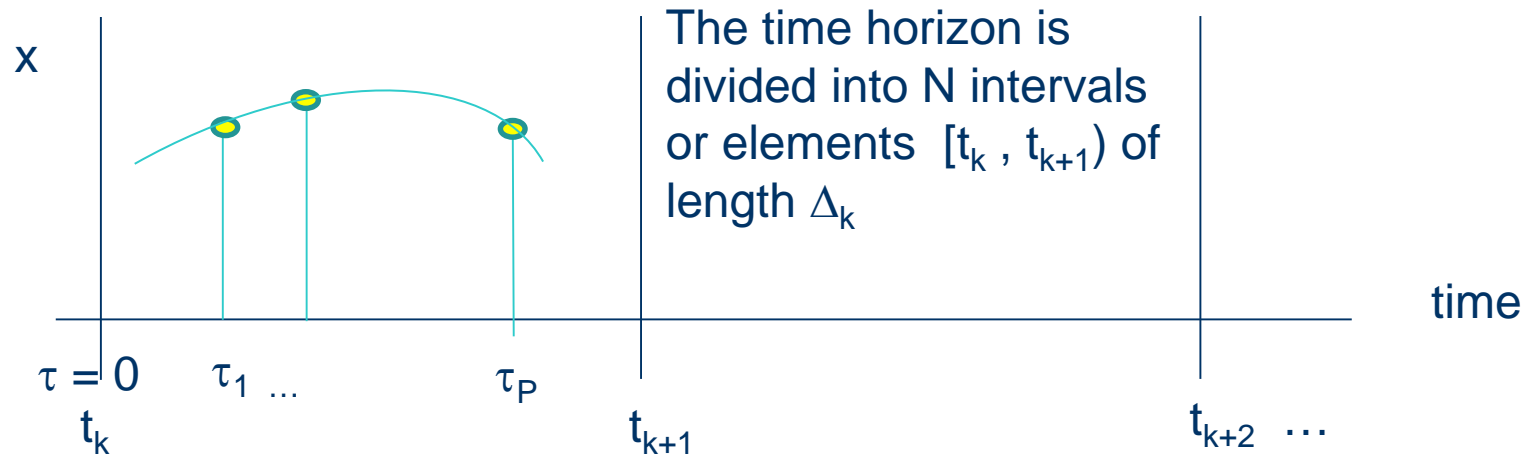
¿nº de  
elementos?

La integración de sistemas stiff usa métodos de paso y estructura variable para mantener el error de integración bajo cotas.

El uso de métodos de paso fijo obliga a usar un gran número de intervalos, resultando en un alto número de ecuaciones y variables y no garantiza la calidad



# Collocation on finite elements



The time evolution of the variables is approximated by polynomial interpolation on the values of the variable on  $P+1$  collocation points located at fixed positions  $\tau_j$  in every element  $k$ . Different methods exist

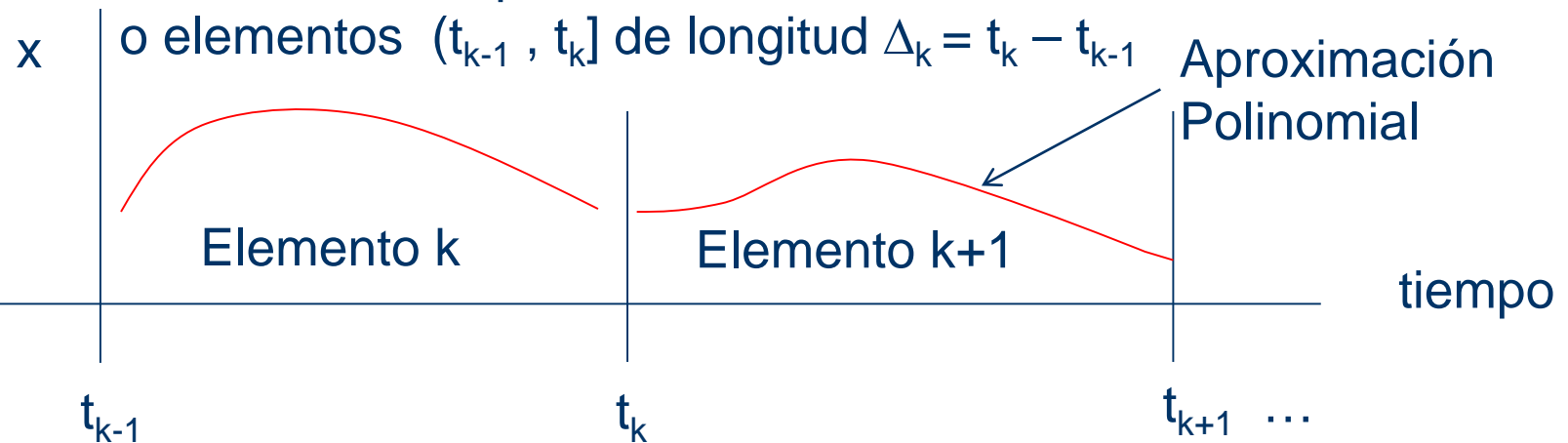
$$\mathbf{x}(t) \approx \sum_{j=0}^P P_j(\tau) \mathbf{x}_{kj}$$

$$t = t_k + \tau \Delta_k \quad \tau \in [0,1)$$

$$\dot{\mathbf{x}}(t) \approx \sum_{j=0}^P \frac{\dot{P}_j(\tau) \mathbf{x}_{kj}}{\Delta_k}$$

# Colocación en elementos finitos

El horizonte temporal se divide en  $K$  intervalos

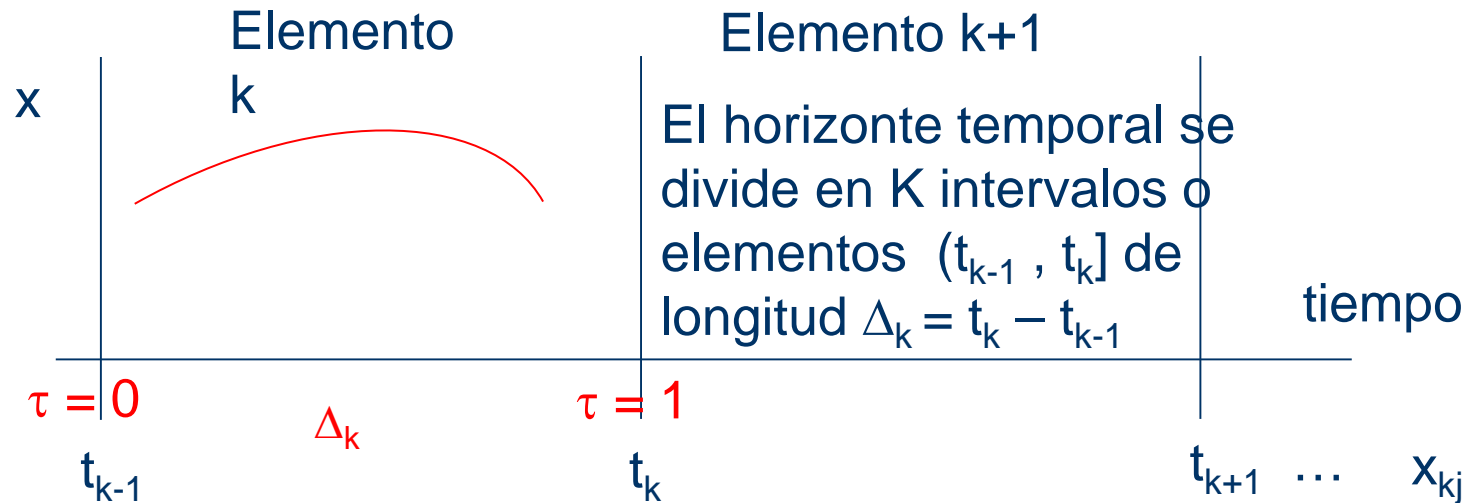


En cada intervalo  $(t_{k-1}, t_k]$  la solución  $x$  se aproxima por una fórmula polinómica. Esto proporciona una aproximación suave en elemento, al tiempo que permite discontinuidades en la señal de control.

Pueden usarse muchos tipos de aproximaciones polinómicas

El número de elementos  $K$  no tiene por qué ser grande

# Colocación en elementos finitos



Una posibilidad es aproximar la evolución temporal de las variables por una combinación lineal de polinomios conocidos  $P_j(\tau)$  de orden  $P$ . Típicamente se usan polinomios de interpolación de Lagrange.

$$\mathbf{x}(t) \approx \sum_{j=0}^P P_j(\tau) \mathbf{x}_{kj}$$

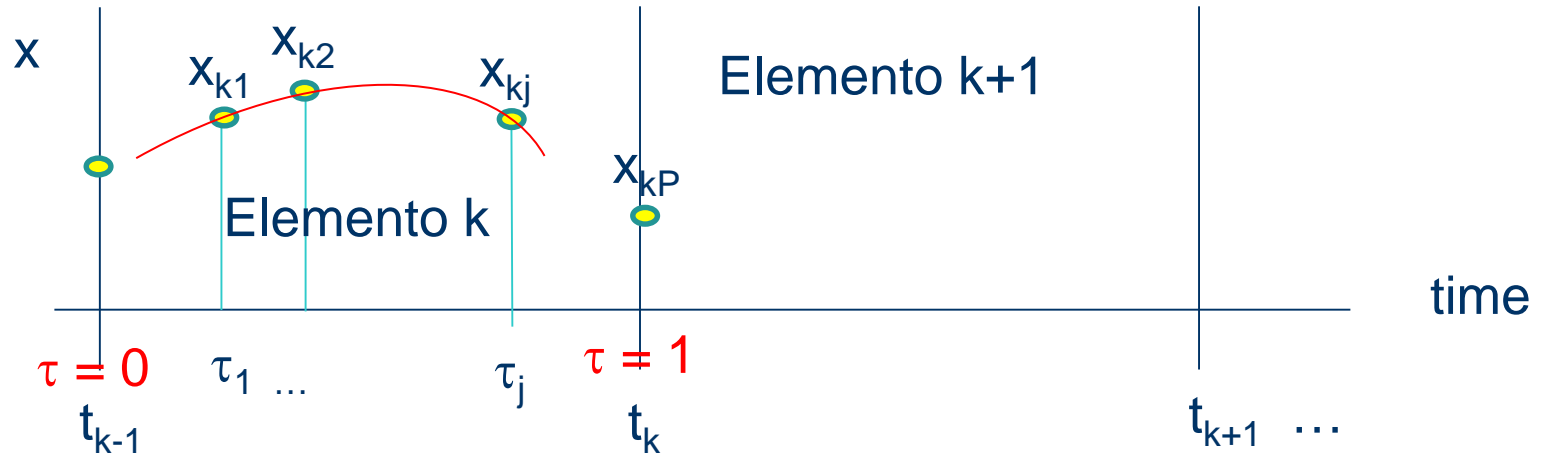
$\mathbf{x}_{kj}$   
parámetros  
a calcular

$$t = t_{k-1} + \tau \Delta_k \quad \tau \in (0,1] \quad k = 1, \dots, K$$

$$\dot{\mathbf{x}}(t) \approx \sum_{j=0}^P \frac{\dot{P}_j(\tau) \mathbf{x}_{kj}}{\Delta_k}$$

$\tau$  Tiempo  
normalizado

# Polinomios de interpolación de Lagrange



$$\mathbf{x}(t) \approx \sum_{j=0}^P P_j(\tau) \mathbf{x}_{kj}$$

$$t = t_{k-1} + \tau \Delta_k \quad \tau \in (0,1]$$

$$\dot{\mathbf{x}}(t) \approx \sum_{j=0}^P \frac{\dot{P}_j(\tau) \mathbf{x}_{kj}}{\Delta_k}$$

$$P_j(\tau) = \prod_{i=0, i \neq j}^P \frac{\tau - \tau_i}{\tau_j - \tau_i}$$

$$\mathbf{x}(t_{kj} = \tau_j) = \mathbf{x}(t_{k-1} + \tau_j \Delta_k) = \mathbf{x}_{kj}$$

Se seleccionan  
P+1 puntos de  
interpolación

$$\tau_0 = 0, \tau_1, \dots, \tau_P$$

$$\tau_i < \tau_{i+1}$$

Los parámetros  $x_{kj}$  tienen un  
significado claro cuando se usan  
los polinomios de Lagrange

# Polinomios de Lagrange

$$P_j(\tau) = \prod_{i=0, i \neq j}^P \frac{\tau - \tau_i}{\tau_j - \tau_i}$$

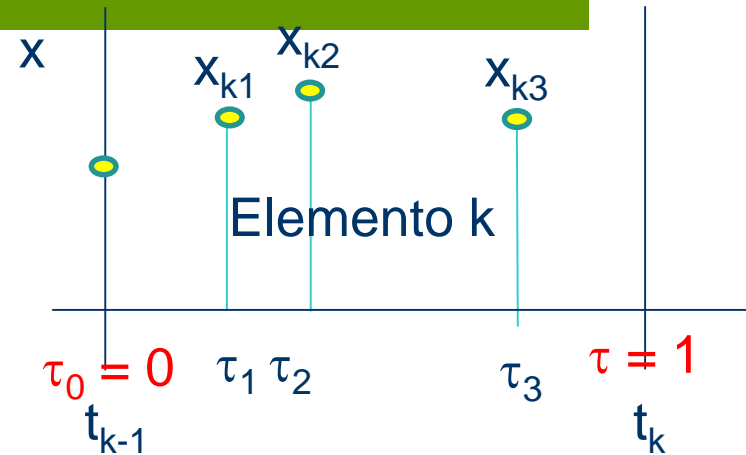
$$P_0 = \frac{\tau - \tau_1}{\tau_0 - \tau_1} \frac{\tau - \tau_2}{\tau_0 - \tau_2} \frac{\tau - \tau_3}{\tau_0 - \tau_3}$$

$$P_1 = \frac{\tau - \tau_0}{\tau_1 - \tau_0} \frac{\tau - \tau_2}{\tau_1 - \tau_2} \frac{\tau - \tau_3}{\tau_1 - \tau_3}$$

$$P_2 = \frac{\tau - \tau_0}{\tau_2 - \tau_0} \frac{\tau - \tau_1}{\tau_2 - \tau_1} \frac{\tau - \tau_3}{\tau_2 - \tau_3}$$

$$P_3 = \frac{\tau - \tau_0}{\tau_3 - \tau_0} \frac{\tau - \tau_1}{\tau_3 - \tau_1} \frac{\tau - \tau_2}{\tau_3 - \tau_2}$$

$$\mathbf{x}(t_{k-1} + \tau_j \Delta_k) = \mathbf{x}_{kj}$$

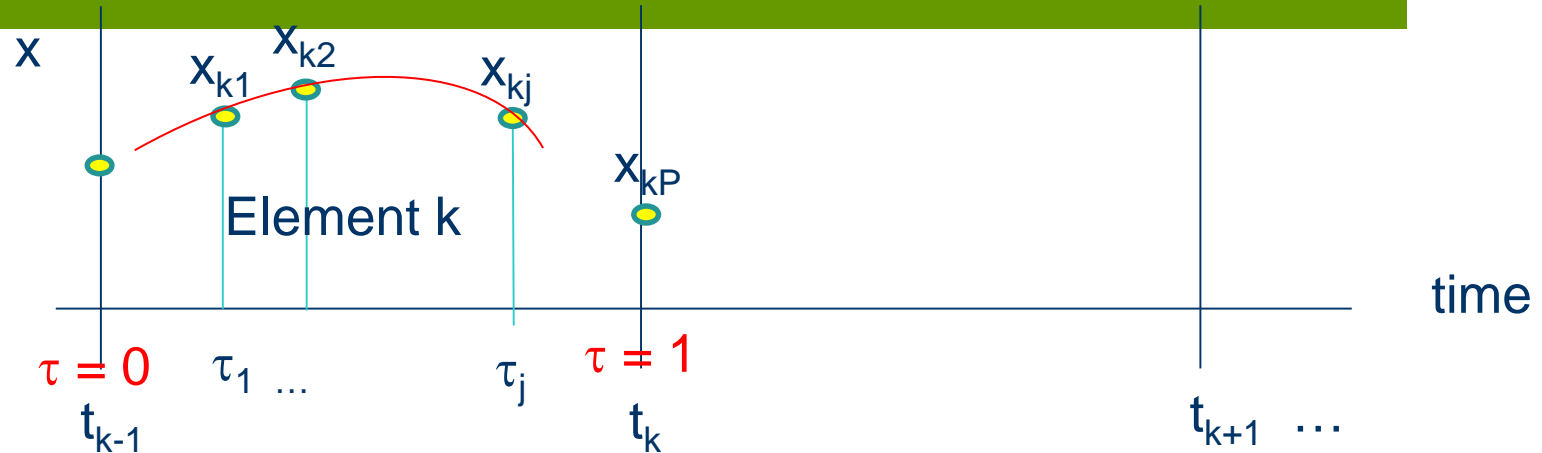


Ejemplo con  $P=3$   $\mathbf{x}(t) \approx \sum_{j=0}^P P_j(\tau) \mathbf{x}_{kj}$

Para  $\tau = \tau_1$   $P_0 = P_2 = P_3 = 0$   $P_1 = 1$

$$\begin{aligned} \mathbf{x}(t_{k-1} + \tau_1 \Delta_k) &= \\ &= P_0 \mathbf{x}_{k0} + P_1 \mathbf{x}_{k1} + P_2 \mathbf{x}_{k2} + P_3 \mathbf{x}_{k3} = \mathbf{x}_{k1} \end{aligned}$$

# Colocación en elementos finitos



Se impone que se satisfagan las ecuaciones DAE en los puntos de colocación.

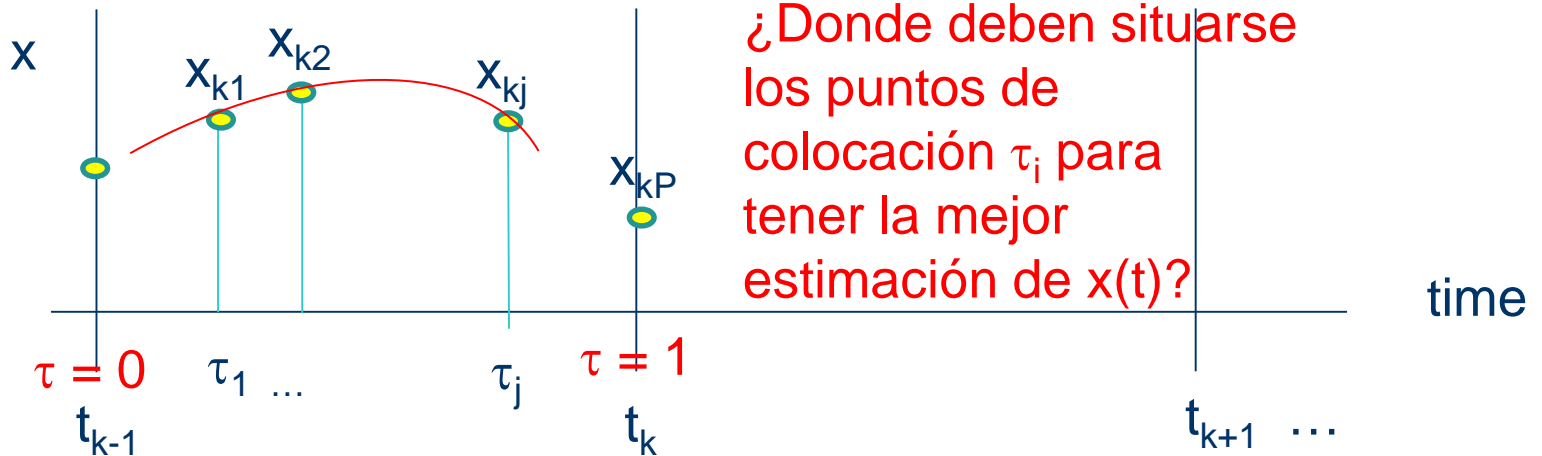
Esta condición proporciona un conjunto de ecuaciones que permiten calcular los coeficientes  $x_{ki}$  desconocidos

$$F(\dot{\mathbf{x}}, \mathbf{x}, \mathbf{u}(\mathbf{p})) = 0$$

$$F\left(\sum_{j=0}^P \frac{\dot{\mathbf{P}}_j(\tau_i) \mathbf{x}_{kj}}{\Delta_k}, \mathbf{x}_{ki}, \mathbf{u}(\mathbf{p})\right) = 0 \quad k = 1, \dots, K$$

Los  $P+1$  puntos de colocación se sitúan en posiciones fijas  $\tau_i$  en cada elemento  $k$ . Existen diferentes métodos para situarlos

# Colocación Ortogonal



$$F\left(\sum_{j=0}^P \frac{\dot{P}_j(\tau_i) \mathbf{x}_{kj}}{\Delta_k}, \mathbf{x}_{ki}, u(p)\right) = 0 \quad \begin{array}{l} k = 1, \dots, K \\ i = 1, \dots, P \end{array}$$

Para reducir el número de polinomios ( $P$ ) se escogen polinomios ortogonales

$$\int_0^1 P_j(\tau) P_i(\tau) d\tau = 0 \quad i \neq j$$

# Colocación Ortogonal

Shifted Gauss–Legendre and Radau roots as collocation points.

De: $P$	$K$	Legendre Roots	Radau Roots
1		0.500000	1.000000
2		0.211325 0.788675	0.333333 1.000000
3		0.112702 0.500000 0.887298	0.155051 0.644949 1.000000
4		0.069432 0.330009 0.669991 0.930568	0.088588 0.409467 0.787659 1.000000
5		0.046910 0.230765 0.500000 0.769235 0.953090	0.057104 0.276843 0.583590 0.860240 1.000000

$\tau_0$  es siempre = 0

Los puntos de colocación  $\tau_i$ ,  $i = 1, \dots, P$  se seleccionan como las raíces de polinomios de tipo Gauss-Jacobi, típicamente:

$$P_P^{\text{Legendre}}(\tau) = \sum_{j=0}^P (-1)^{P-j} \tau^j \gamma_j$$

$$\gamma_0 = 1$$

$$\gamma_j = \frac{(P-j+1)(P+j)}{j^2}$$

Dan mas exactitud

$$P_P^{\text{Radau}}(\tau) = \sum_{j=0}^P (-1)^{P-j} \tau^j \gamma_j$$

$$\gamma_0 = 1$$

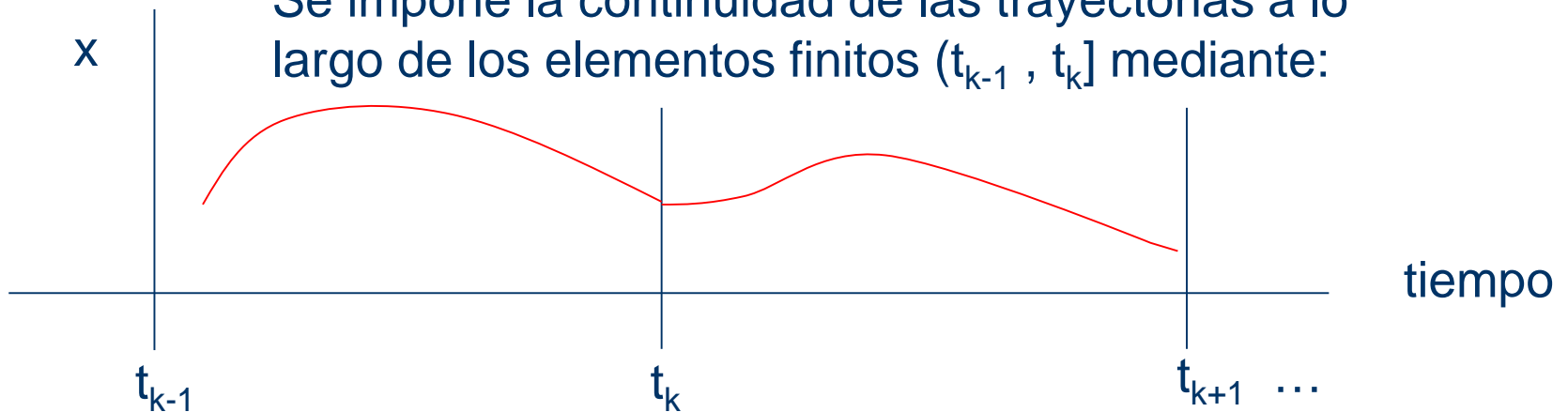
$$\gamma_j = \frac{(P-j+1)(P+j+1)}{j^2}$$

Dan mas robustez



# Colocación Ortogonal

Se impone la continuidad de las trayectorias a lo largo de los elementos finitos  $(t_{k-1}, t_k]$  mediante:



$$F\left(\sum_{j=0}^P \frac{\dot{P}_j(\tau_i) \mathbf{x}_{kj}}{\Delta_k}, \mathbf{x}_{ki}, \mathbf{u}(p)\right) = 0 \quad \begin{array}{l} k = 1, \dots, K \\ i = 1, \dots, P \end{array}$$

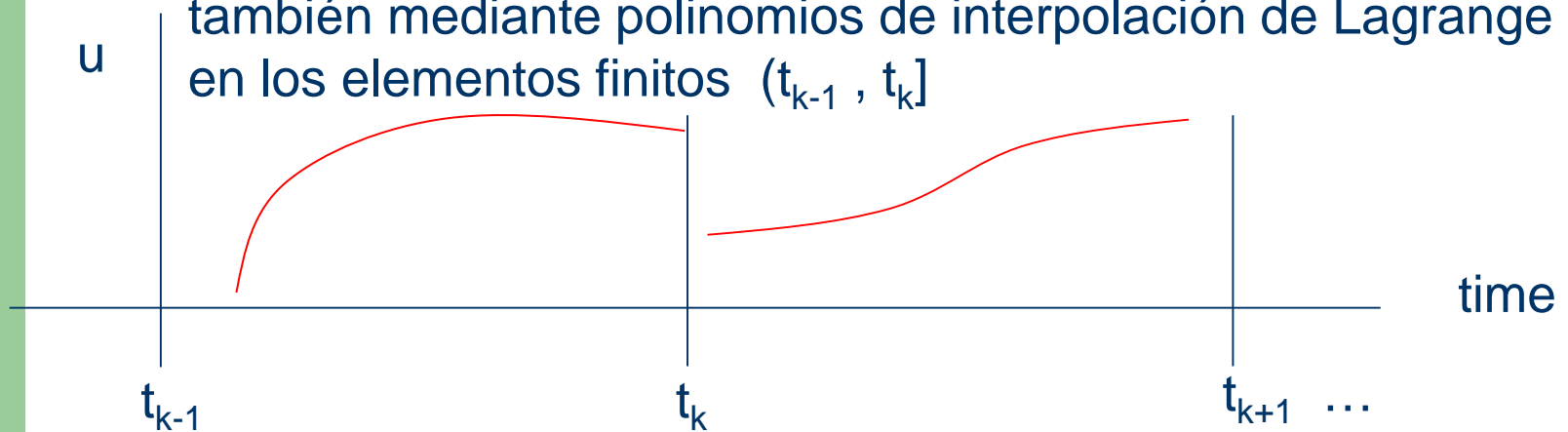
En lugar de estas ecuaciones, en los puntos  $\tau_0 = 0$  se usa la continuidad de los estados, y en  $t = 0$  las condiciones iniciales para generar ecuaciones que las sustituyan y que garanticen soluciones acorde a lo deseado

$$\mathbf{x}(t_k) = \mathbf{x}_{k+1,0} = \mathbf{x}_{k,P}$$

$$\mathbf{x}(t_0) = \mathbf{x}_{10} = \mathbf{x}_0$$

# Colocación Ortogonal

Si se desea, las variables de control pueden representarse también mediante polinomios de interpolación de Lagrange en los elementos finitos  $(t_{k-1}, t_k]$



$$\mathbf{u}(t) \approx \sum_{j=1}^P \bar{P}_j(\tau) \mathbf{u}_{kj}$$

$$\bar{P}_j(\tau) = \prod_{i=1, i \neq j}^P \frac{\tau - \tau_i}{\tau_j - \tau_i}$$

$$t = t_{k-1} + \tau \Delta_k \quad \tau \in (0,1]$$

**No se impone** la continuidad de las trayectorias de control en los elementos finitos  $(t_{k-1}, t_k]$

Pueden usarse métodos simultáneos de optimización con sistemas inestables

# Ejemplo

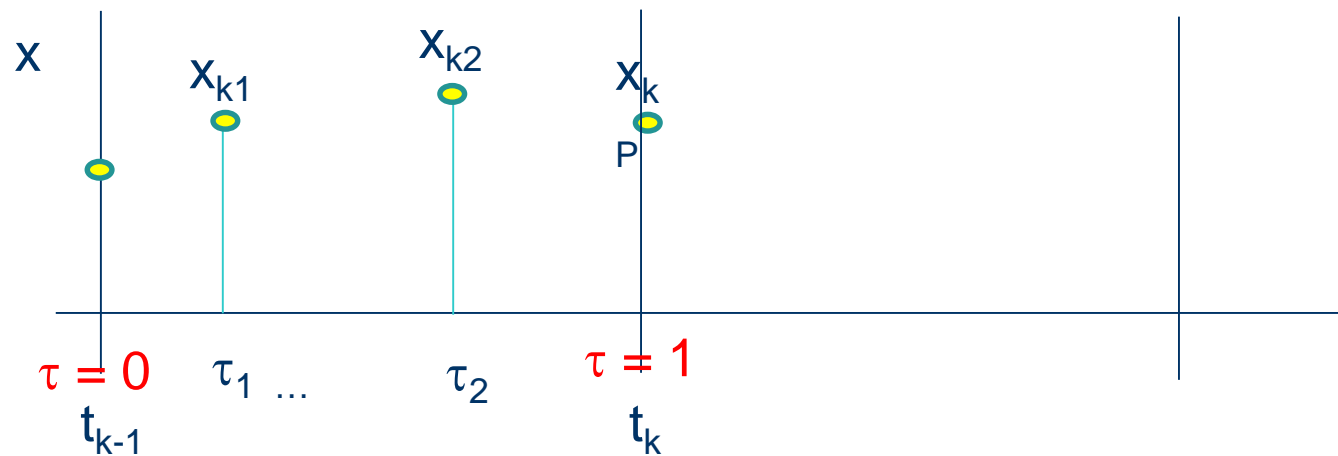
Integrar entre  $t = 0$  y  $1$

$$\dot{x} = x^2 - 2x + 1 \quad x(0) = -3$$

Se seleccionan  $K = 2$  elementos finitos de igual tamaño

$$\Delta_k = (1 - 0)/2 = 0.5$$

$P = 3$  puntos de colocación



Los puntos de colocación de Radau para  $P = 3$  son:

$$\tau_0 = 0 \quad \tau_1 = 0.155051 \quad \tau_2 = 0.644949 \quad \tau_3 = 1$$

# Ejemplo

Los puntos de colocación de Radau para  $P = 3$  son:  
 $\tau_0 = 0$   $\tau_1 = 0.155051$   $\tau_2 = 0.644949$   $\tau_3 = 1$

$$P_j(\tau) = \prod_{i=0, i \neq j}^P \frac{\tau - \tau_i}{\tau_j - \tau_i}$$

$$P_0 = \frac{\tau - \tau_1}{\tau_0 - \tau_1} \frac{\tau - \tau_2}{\tau_0 - \tau_2} \frac{\tau - \tau_3}{\tau_0 - \tau_3} = -10\tau^3 + 18\tau^2 - 9\tau + 1$$

$$P_1 = \frac{\tau - \tau_0}{\tau_1 - \tau_0} \frac{\tau - \tau_2}{\tau_1 - \tau_2} \frac{\tau - \tau_3}{\tau_1 - \tau_3} = 15.5808\tau^3 - 25.6296\tau^2 + 10.0488\tau$$

$$P_2 = \frac{\tau - \tau_0}{\tau_2 - \tau_0} \frac{\tau - \tau_1}{\tau_2 - \tau_1} \frac{\tau - \tau_3}{\tau_2 - \tau_3} = -8.9141\tau^3 + 10.2963\tau^2 - 1.3821\tau$$

$$P_3 = \frac{\tau - \tau_0}{\tau_3 - \tau_0} \frac{\tau - \tau_1}{\tau_3 - \tau_1} \frac{\tau - \tau_2}{\tau_3 - \tau_2} = 3.3333\tau^3 - 2.6667\tau^2 + 0.3333\tau$$

$$\mathbf{x}(t_{k-1} + \tau_j \Delta_k) = \mathbf{x}_{kj} \quad \mathbf{x}(t) \approx \sum_{j=0}^P P_j(\tau) \mathbf{x}_{kj} \quad t = t_{k-1} + \tau \Delta_k \quad \tau \in (0,1]$$

# Ejemplo

Los puntos de colocación de Radau para  $P = 3$  son:  
 $\tau_0 = 0$   $\tau_1 = 0.155051$   $\tau_2 = 0.644949$   $\tau_3 = 1$

$$\dot{\mathbf{x}}(t) \approx \sum_{j=0}^P \frac{\dot{P}_j(\tau) \mathbf{x}_{kj}}{\Delta_k}$$

$$\dot{P}_0(\tau) = -30\tau^2 + 36\tau - 9$$

$$\dot{P}_1(\tau) = 46.7423\tau^2 - 51.2592\tau + 10.0488$$

$$\dot{P}_2(\tau) = -26.7423\tau^2 + 20.5925\tau - 1.3821$$

$$\dot{P}_3(\tau) = 10\tau^2 - 5.3333\tau + 0.3333$$

$$\mathbf{x}(t_{k-1} + \tau_j \Delta_k) = \mathbf{x}_{kj}$$

$$t = t_{k-1} + \tau \Delta_k \quad \tau \in (0,1]$$

$$\dot{x} = x^2 - 2x + 1 \quad x(0) = -3$$

$$\sum_{j=0}^3 \frac{\dot{P}_j(\tau) \mathbf{x}_{kj}}{0.5} = x^2 - 2x + 1$$

$$k = 1, 2$$

# Ejemplo

$$\dot{x} = x^2 - 2x + 1 \quad x(0) = -3 \quad \longrightarrow \quad \sum_{j=0}^3 \frac{\dot{P}_j(\tau) \mathbf{x}_{kj}}{0.5} = \mathbf{x}^2 - 2\mathbf{x} + 1 \quad k = 1, 2$$

En los puntos de colocación  $\tau_i$  :

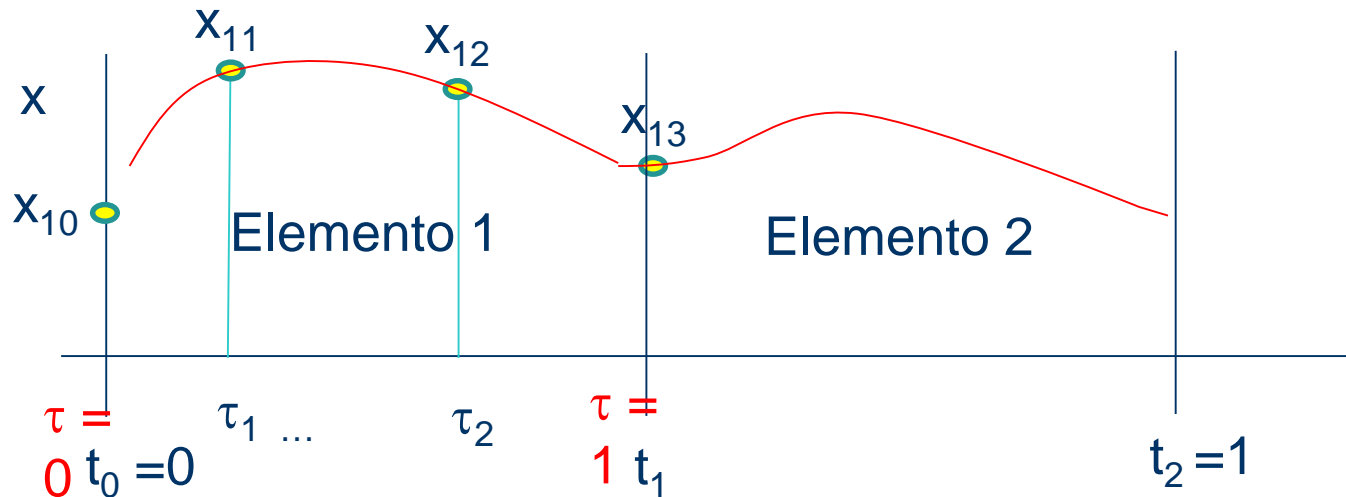
$$\sum_{j=0}^3 \frac{\dot{P}_j(\tau_i) \mathbf{x}_{kj}}{0.5} = \mathbf{x}_{ki}^2 - 2\mathbf{x}_{ki} + 1 \quad \begin{matrix} k = 1, 2 \\ i = 1, \dots, 3 \end{matrix}$$

$$\begin{aligned} & (-30\tau_i^2 + 36\tau_i - 9)x_{10} + (46.7423\tau_i^2 - 51.2592\tau_i + 10.0488)x_{11} + \\ & + (-26.7423\tau_i^2 + 20.5925\tau_i - 1.3821)x_{12} + (10\tau_i^2 - 5.3333\tau_i + 0.3333)x_{13} = \\ & = 0.5(x_{1i}^2 - 2x_{1i} + 1) \quad i = 1, 2, 3 \end{aligned}$$

$$\begin{aligned} & (-30\tau_i^2 + 36\tau_i - 9)x_{20} + (46.7423\tau_i^2 - 51.2592\tau_i + 10.0488)x_{21} + \\ & + (-26.7423\tau_i^2 + 20.5925\tau_i - 1.3821)x_{22} + (10\tau_i^2 - 5.3333\tau_i + 0.3333)x_{23} = \\ & = 0.5(x_{2i}^2 - 2x_{2i} + 1) \quad i = 1, 2, 3 \end{aligned}$$

8 incógnitas, 6 ecuaciones

# Ejemplo



$$\mathbf{x}(t_k) = \mathbf{x}_{k+1,0} = \mathbf{x}_{k,P} = \sum_{j=0}^P P_j(1) \mathbf{x}_{k,j}$$

$$\mathbf{x}(0.5) = \mathbf{x}_{20} = \mathbf{x}_{13} = \sum_{j=0}^3 P_j(1) \mathbf{x}_{1j}$$

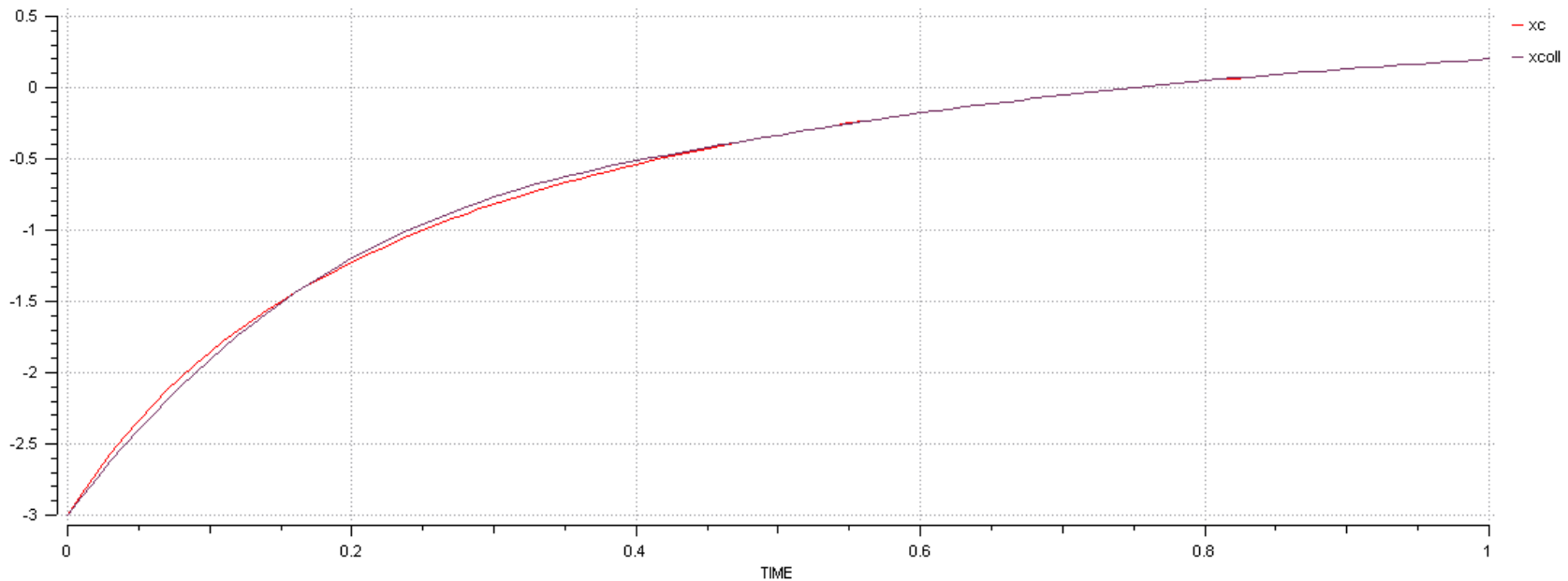
$$\mathbf{x}(t_0) = \mathbf{x}_{10} = \mathbf{x}_0$$

$$\mathbf{x}(0) = \mathbf{x}_{10} = -3$$

8 incógnitas, 8  
ecuaciones

Las condiciones iniciales y de continuidad  
proporcionan las otras dos ecuaciones

# Ejemplo

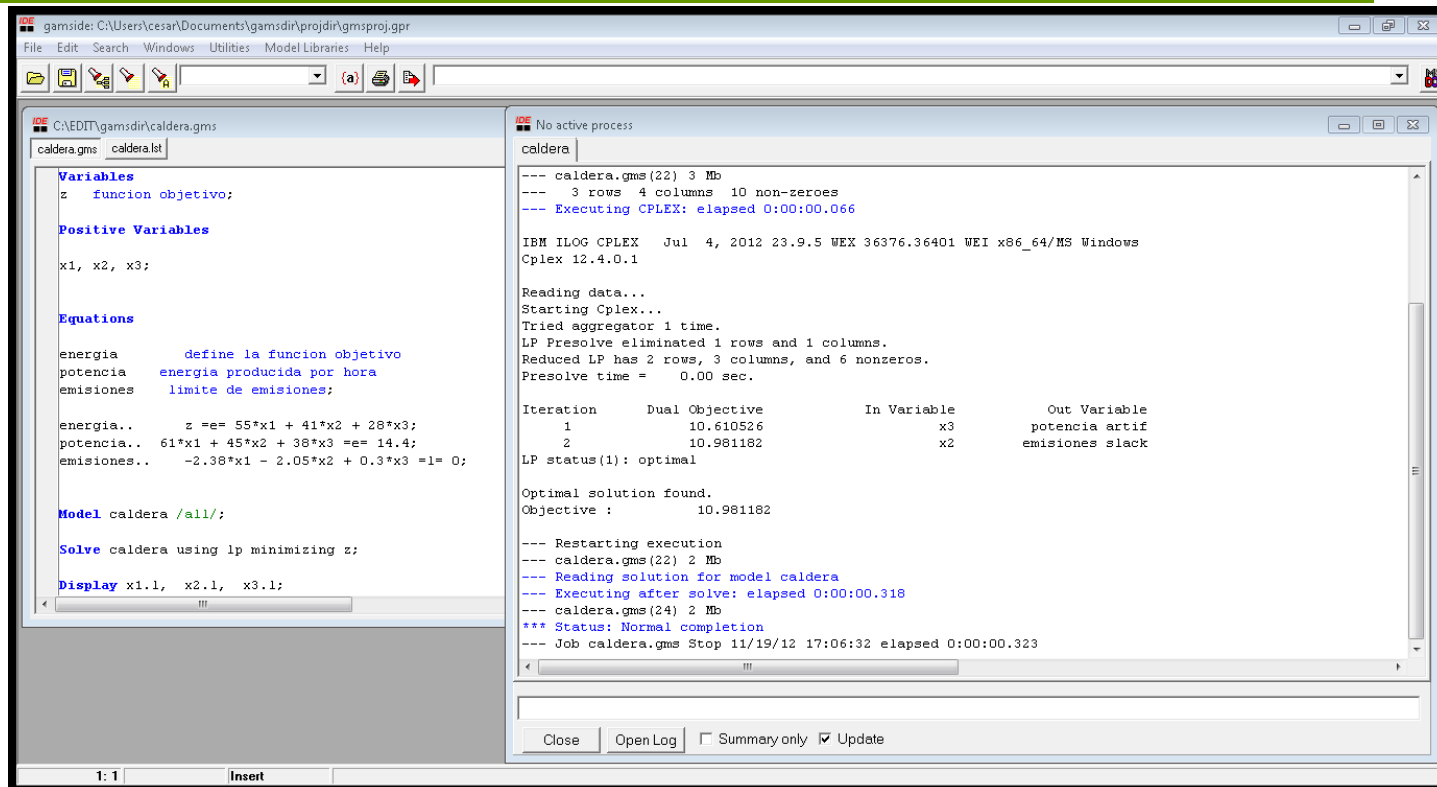


$$\dot{x} = x^2 - 2x + 1 \quad x(0) = -3$$

Respuestas analítica y obtenida por colocación ortogonal



# Software: GAMS



The screenshot displays the GAMS IDE interface. The left pane shows the model code for 'caldera.gms', and the right pane shows the execution log.

**Model Code (Left Pane):**

```
Variables
z  funcion objetivo;

Positive Variables
x1, x2, x3;

Equations
energia  define la funcion objetivo
potencia energia producida por hora
emisiones limite de emisiones;

energia..  z =e= 55*x1 + 41*x2 + 28*x3;
potencia.. 61*x1 + 45*x2 + 38*x3 =e= 14.4;
emisiones.. -2.38*x1 - 2.05*x2 + 0.3*x3 =1= 0;

Model caldera /all/;

Solve caldera using lp minimizing z;

Display x1.l, x2.l, x3.l;
```

**Execution Log (Right Pane):**

```
--- caldera.gms (22) 3 Mb
--- 3 rows 4 columns 10 non-zeroes
--- Executing CPLEX: elapsed 0:00:00.066

IBM ILOG CPLEX Jul 4, 2012 23:9.5 WEX 36376.36401 WEI x86_64/MS Windows
Cplex 12.4.0.1

Reading data...
Starting Cplex...
Tried aggregator 1 time.
LP Presolve eliminated 1 rows and 1 columns.
Reduced LP has 2 rows, 3 columns, and 6 nonzeros.
Presolve time = 0.00 sec.

Iteration   Dual Objective      In Variable      Out Variable
1           10.610526          x3               potencia artif
2           10.981182          x2               emisiones slack

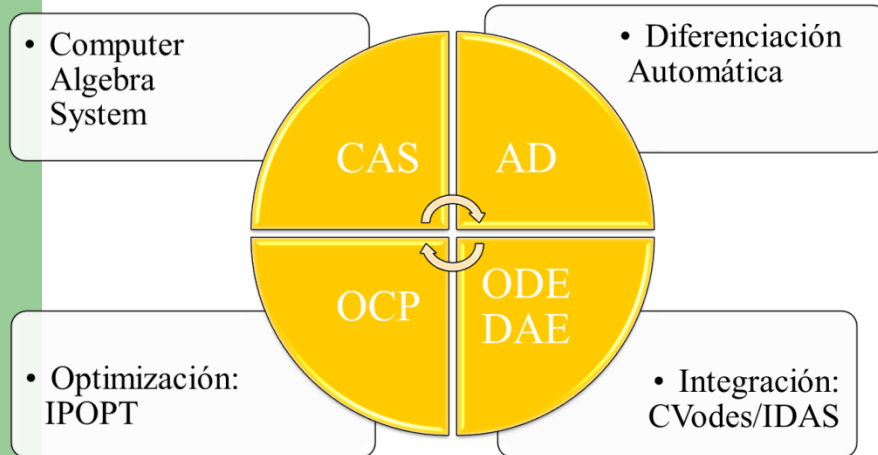
LP status(1): optimal

Optimal solution found.
Objective : 10.981182

--- Restarting execution
--- caldera.gms (22) 2 Mb
--- Reading solution for model caldera
--- Executing after solve: elapsed 0:00:00.318
--- caldera.gms (24) 2 Mb
*** Status: Normal completion
--- Job caldera.gms Stop 11/19/12 17:06:32 elapsed 0:00:00.323
```

Entornos de modelado y optimización como GAMS, AIMMS, XPRESS, Gurobi,... pueden usarse tras la discretización

# Software



Solución eficiente de problemas de gran escala

Pero no soporta:

- Discontinuidades
- Optimización mixta-entera

Problemas de memoria

Entorno pobre de modelado

Computational Infrastructure for Operations Research (COIN-OR) Open source codes

Sensibilidades paramétricas

**CasADi** es un entorno simbólico para optimización numérica que facilita la discretización e implementa diferenciación automática (gradientes y Hessianos).

Genera código C e implementa interfaces a códigos DAE y de optimización como SUNDIALS, IPOPT etc.

Se gestiona desde una interfaz con Python/Matlab

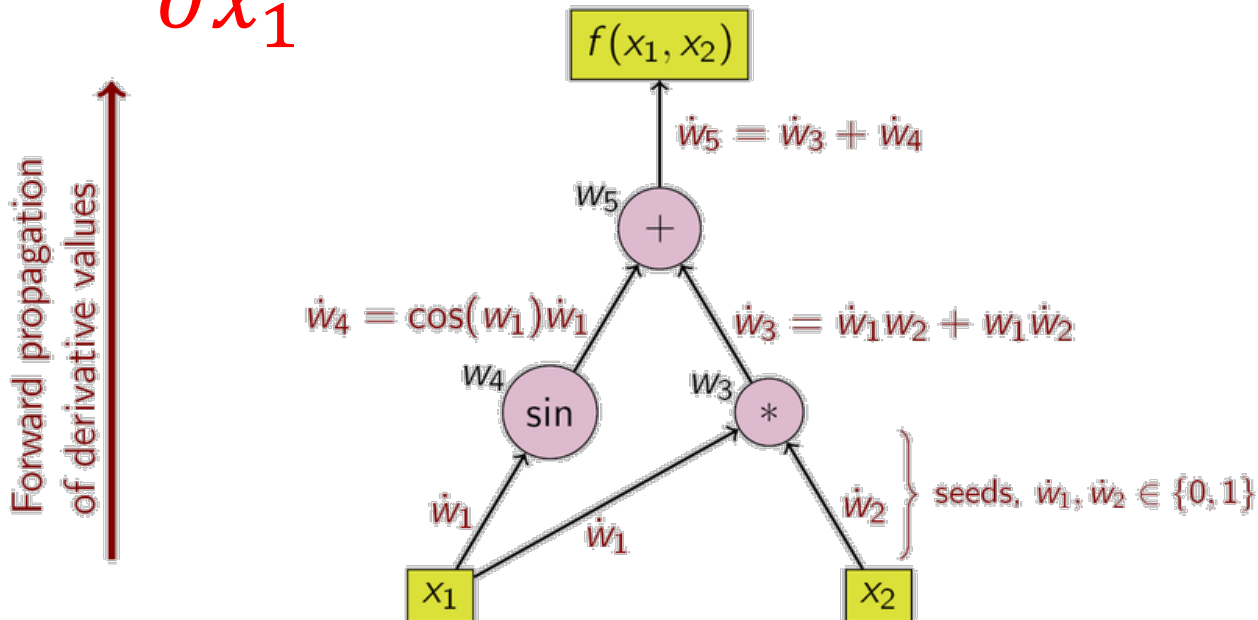
# Diferenciación Automática

Ejemplo::

$$f = x_1 x_2 + \sin(x_1)$$

$$¿ \frac{\partial f}{\partial x_1} ?$$

Assignment	Derivatives
$w_1 = x_1$	$w_1' = 1$ ( <i>seed</i> )
$w_2 = x_2$	$w_2' = 0$ ( <i>seed</i> )
$w_3 = w_1 w_2$	$w_3' = w_1' w_2 + w_1 w_2' = x_2$
$w_4 = \sin(w_1)$	$w_4' = \cos(w_1) w_1' = \cos(x_1)$
$w_5 = w_3 + w_4$	$w_5' = w_3' + w_4' = x_2 + \cos(x_1)$



# Optimal control

Classical optimal control theory has its roots in the **calculus of Variations**.

Typical problems are formulated as:

$$\min_{\mathbf{u}(t)} J(\mathbf{u}) = \phi(\mathbf{x}(t_f)) + \int_{t_0}^{t_f} C(\mathbf{x}, \mathbf{u}) dt$$

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}, t), \quad \mathbf{x}(t_0) = \mathbf{x}_0$$

$$t_0, t_f, \mathbf{x}_0 \quad \text{specified}$$

The Lagrange multipliers approach and variational principle can be used to solve the problem. As the constraints are dynamic, the Lagrange multiplier vector  $\lambda(t)$  is a function of time.

$$\min_{\mathbf{u}(t), \lambda(t)} \bar{J} = \phi(\mathbf{x}(t_f)) + \int_{t_0}^{t_f} \{C(\mathbf{x}, \mathbf{u}) + \lambda(t)' [\mathbf{f}(\mathbf{x}, \mathbf{u}, t) - \dot{\mathbf{x}}]\} dt$$

# Hamiltonian

Using the **Hamiltonian**, defined as:

$$H(t) = C(\mathbf{x}, \mathbf{u}) + \lambda(t)' \mathbf{f}(\mathbf{x}, \mathbf{u}, t)$$

$$\begin{aligned} \bar{J} &= \phi(\mathbf{x}(t_f)) + \int_{t_0}^{t_f} \{C(\mathbf{x}, \mathbf{u}) + \lambda(t)' [\mathbf{f}(\mathbf{x}, \mathbf{u}, t) - \dot{\mathbf{x}}]\} dt = \\ &= \phi(\mathbf{x}(t_f)) + \int_{t_0}^{t_f} \{H(t) - \lambda(t)' \dot{\mathbf{x}}\} dt = (\text{integrating by parts } \lambda \dot{\mathbf{x}}) \\ &= \phi(\mathbf{x}(t_f)) - \lambda(t_f)' \mathbf{x}(t_f) + \lambda(t_0)' \mathbf{x}(t_0) + \int_{t_0}^{t_f} \{H(t) + \dot{\lambda}(t)' \mathbf{x}\} dt \end{aligned}$$

# NOC

$$\bar{J} = \phi(\mathbf{x}(t_f)) - \lambda(t_f)' \mathbf{x}(t_f) + \lambda(t_0)' \mathbf{x}(t_0) + \int_{t_0}^{t_f} \left\{ H(t) + \dot{\lambda}(t)' \mathbf{x} \right\} dt$$

for optimality :

$$\left. \frac{\partial \phi}{\partial \mathbf{x}} \frac{\partial \mathbf{x}}{\partial \mathbf{u}} \right|_{t_f} - \lambda(t_f)' \left. \frac{\partial \mathbf{x}}{\partial \mathbf{u}} \right|_{t_f} + \int_{t_0}^{t_f} \left\{ \frac{\partial H}{\partial \mathbf{x}} \frac{\partial \mathbf{x}}{\partial \mathbf{u}} + \frac{\partial H}{\partial \mathbf{u}} + \dot{\lambda}(t)' \frac{\partial \mathbf{x}}{\partial \mathbf{u}} \right\} dt = 0$$

$$\dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}, t)$$

Now, by choosing:

$$\dot{\lambda}(t)' = - \frac{\partial H}{\partial \mathbf{x}} \quad \lambda(t_f)' = \left. \frac{\partial \phi}{\partial \mathbf{x}} \right|_{t_f} \quad \frac{\partial H}{\partial \mathbf{u}} = 0 \quad \mathbf{x}(t_0) \text{ given}$$

The NOC are always satisfied

# NOC

The NOC in terms of the Hamiltonian are given by:

$$\begin{array}{lll} \dot{\mathbf{x}} = \mathbf{f}(\mathbf{x}, \mathbf{u}, t) & \mathbf{x}(t_0) = \mathbf{x}_0 & \mathbf{H} = \mathbf{C} + \boldsymbol{\lambda}' \mathbf{f}(\mathbf{x}, \mathbf{u}, t) \\ \dot{\boldsymbol{\lambda}}(t)' = -\frac{\partial \mathbf{H}}{\partial \mathbf{x}} & \boldsymbol{\lambda}(t_f)' = \frac{\partial \phi}{\partial \mathbf{x}} \Big|_{t_f} & \frac{\partial \mathbf{H}}{\partial \mathbf{u}} = 0 \end{array}$$

This is a TPBVP as part of the boundary conditions of the differential equations are given at  $t_f$  and part at  $t_0$

Positive definite Hessian is required for sufficiency

Similar equations result for other formulations such as terminal constraints, free final time, etc.